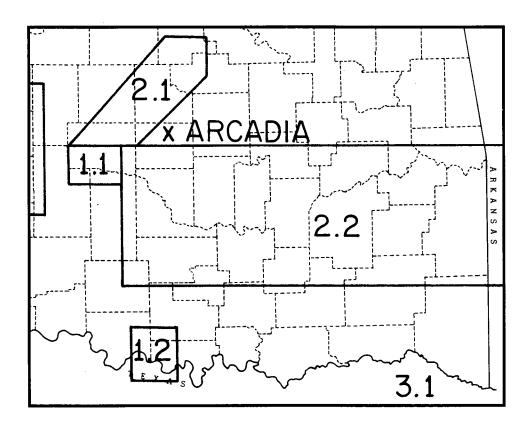


Oklahoma Geological Survey 1985

# Expected Earthquake Ground-Motion Parameters at the Arcadia, Oklahoma, Dam Site

James E. Lawson, Jr.



# EXPECTED EARTHQUAKE GROUND-MOTION

PARAMETERS AT THE ARCADIA, OKLAHOMA, DAM SITE

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September 1980

Final report submitted to
U.S. Army Corps of Engineers
Tulsa District
Contract P.O. No. DACW56-80-M-0660

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## ADVANCE SUMMARY

A study of earthquake distribution and intensity values in Oklahoma was used to divide Oklahoma and parts of the adjacent states into six seismic-source zones. These zones, in order of decreasing seismic activity, embrace certain areas herein referred to as central Oklahoma (also referred to as zone 1.1), south-central Oklahoma (zone 1.2), north-central Oklahoma (zone 2.1), southeast Oklahoma (zone 2.2), west-central Oklahoma (zone 2.3), and residual (an area that encompasses all remaining parts of the State, (zone 3.1). The proposed Arcadia dam site, 30 km northeast of Oklahoma City, is within zone 3.1, the least active zone, and is nearly 35 km from the nearest part of zone 1.1 and is less than 15 km from the nearest part of zones 2.1 and 2.2 (see fig. 2).

For zone 1.1, the largest earthquake magnitude (M) expected in a given number of years (y) was computed from the following expression:

$$M = 2.72 - 0.880 \log(1/y)$$
.

This equation was used to determine expected earthquake magnitudes for various time intervals. For the corresponding time periods of 100, 200, 500, 1000, and 2000 years, the computed magnitudes are 4.5, 4.8, 5.1, 5.4, and 5.6, respectively.

A probabilistic estimate indicates that an earthquake in zone 1.1, 46 km away from Arcadia, would cause the largest ground motion at the dam site. The earthquake-magnitude values calculated for the selected time intervals were used to compute expected horizontal ground accelerations and horizontal ground velocities at the dam site. The values are listed below.

Period (years)	Magnitude (M)	Site acceleration (% of g)	Site velocity (cm/sec)		
100	4.5	3.0	0.8		
200	4.8	4.2	1.5		
500	5.1	6.4	3.3		
1000	5.4	8.7	6.0		
2000	5.6	12.0	11.2		

#### INTRODUCTION

The U.S. Army Corps of Engineers is currently investigating a location near Arcadia in central Oklahoma as a potential dam site (fig. 1). The proposed Arcadia site, on the Deep Fork of the North Canadian River, is about 12 km northeast of Oklahoma City.

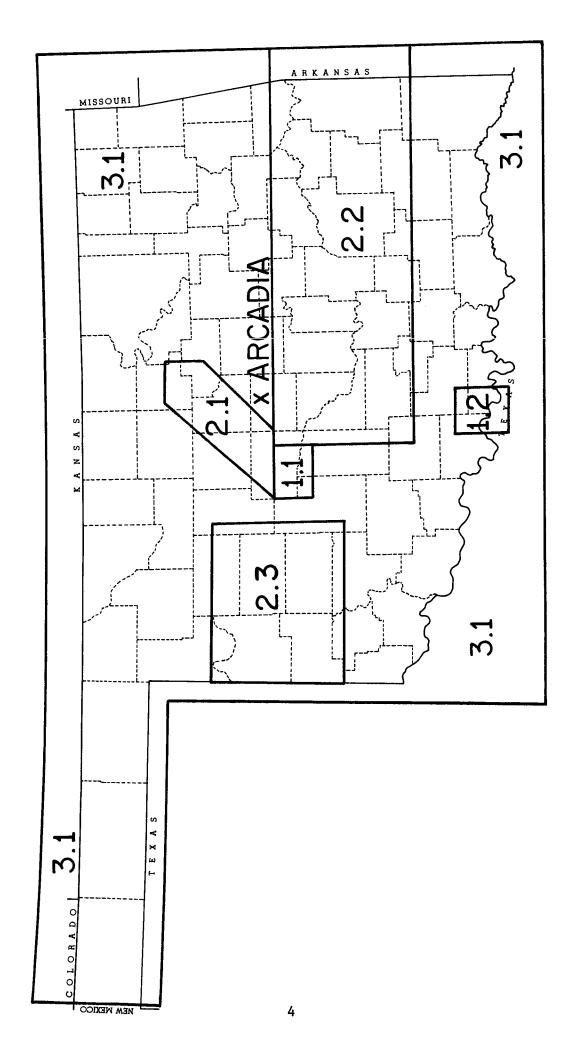
The present report summarizes a study to determine the largest earthquake-generated ground motion that would probably occur at the Arcadia dam site over various periods of time. The ground motion is described in terms of the maximum horizontal ground velocity and the maximum horizontal ground acceleration. These two parameters are evaluated for periods of 100, 200, 500, 1000, and 2000 years, and equivalent Modified Mercalli intensity at the proposed dam site is calculated for each period. Also, the magnitude of the earthquake expected to cause the largest ground motion, and the distance of that earthquake from the site, are tabulated for each of these time periods.

This study takes into account all known historical earthquakes capable of causing significant ground motion at the Arcadia site. For Oklahoma and nearby areas, felt historical earthquakes and smaller instrumentally located earthquakes are grouped into six source zones shown in figure 2. Magnitude-frequency relations were determined for each zone, and these were used to evaluate the expected Arcadia-site ground motion.

#### DATA BASE

A new earthquake data base was assembled in order to evaluate earthquake risk at the Arcadia dam site. The new data base also includes all earthquakes that could possibly have an effect on any site within the State of Oklahoma. The data base was conveniently subdivided into four main parts. These four parts and the sources of information for each part are listed as follows:

PART I - Includes all earthquakes known to have occurred in Oklahoma through the end of 1979.



Index map showing seismic-source zones and the Arcadia dam-site project. Fig. 1.

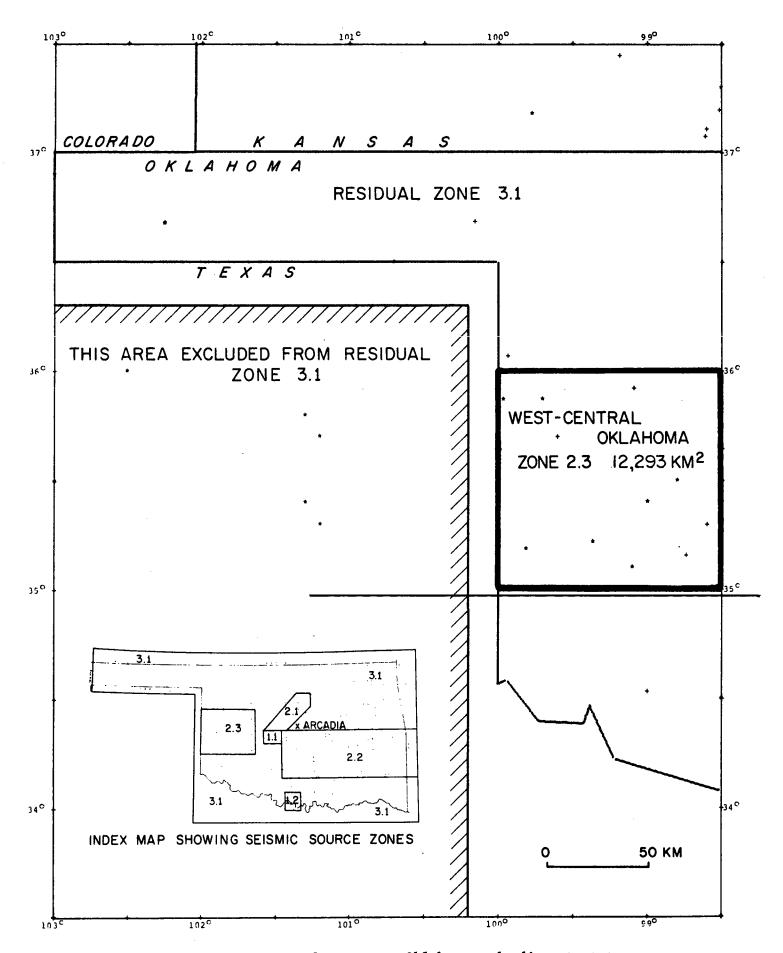


Fig. 2a. Seismic-source zones for western Oklahoma and adjacent states.

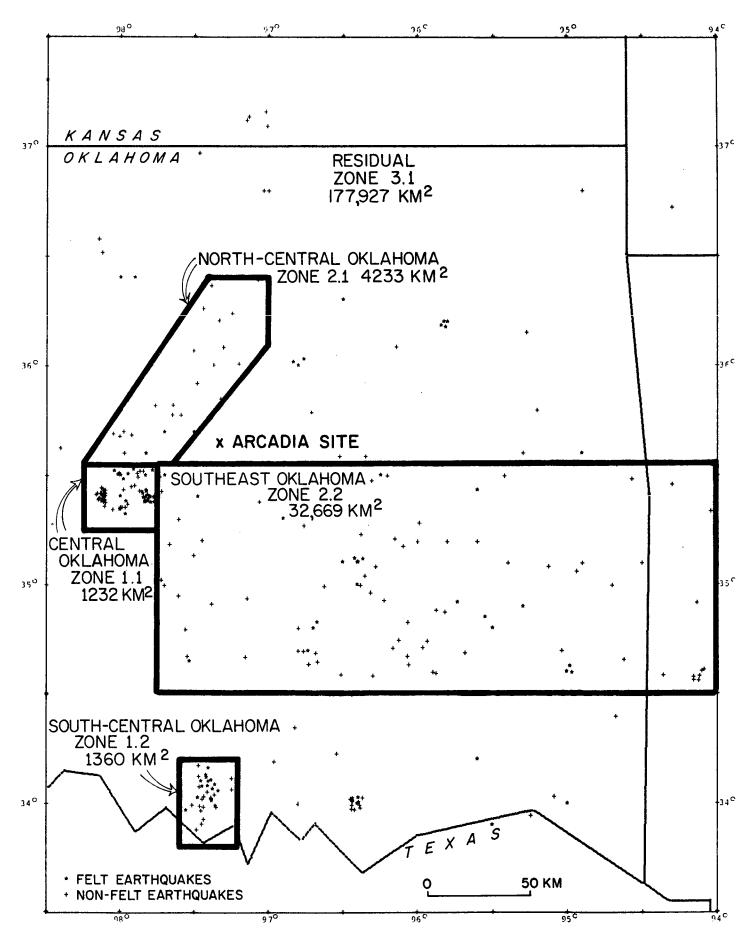


Fig. 2b. Seismic-source zones for eastern Oklahoma and adjacent states.

Sources: Ia - Lawson, J.E., Jr., Dubois, R.L., Foster, P.H., and Luza, K.V., 1979, Earthquake map of Oklahoma (with accompanying text and catalog): Oklahoma Geological Survey Map GM-19, 15 pages, map scale 1:750,000. (Contains all known Oklahoma earthquakes through the end of 1978.)

Ib - Lawson, J.E., Jr., and Luza, K.V., 1980, Oklahoma earthquakes, 1979: Oklahoma Geology Notes, v. 40, p. 95-105.

PART II - Includes all earthquakes not listed in Part I with an intensity (Modified Mercalli) of V or greater that have occurred between 32° and 44° north latitude and 92° and 104° west longitude.

Sources (for earthquakes not already included in Part I): IIa - Coffman, J.L., and von Hake, C.A. (editors), 1973, Earthquake history of the United States, revised edition (through 1970): NOAA publication 41-1, 208 p.

IIb - Coffman, J.L., 1979, Earthquake history of the United States (1971-76 supplement): NOAA and USGS joint publication 41-1, 41 p.

IIc - DuBois, S.M., and Wilson, F.W., 1978, A revised and augmented list of earthquake intensities for Kansas 1867-1977: U.S. Nuclear Regulatory Commission NUREG/CR-0294, 56 p. (Used only for earthquakes not found in sources IIa and IIb.)

IId - Burchett, R.R., 1979, Earthquakes in Nebraska: University of Nebraska Conservation and Survey Division Education Circular 4, 20 p. (Used only for earthquakes not found in sources IIa and IIb.)

PART III - Includes small (MM Intensity V) earthquakes located by the Kansas, Nebraska, and Oklahoma networks in the States of Kansas, Nebraska, Missouri, Texas, and Arkansas for the inclusive period 1977-79.

Sources: IIIa - Luza, K.V., DuBois, R.L., Lawson, J.E., Jr., Foster, Paul, and Koff, Leonid, 1978, Seismicity and tectonic relationships of the Nemaha Uplift in Oklahoma: U.S. Nuclear Regulatory Commission NUREG/CR-0050, 67 p.

IIIb - Luza, K.V., and Lawson, J.E., Jr., 1979, Seismicity and tectonic relationships of the Nemaha Uplift in Oklahoma, Part II: U.S. Nuclear Regulatory Commission NUREG/CR-0875, 81 p.

IIIc - Luza, K.V., and Lawson, J.E., Jr., 1980, Seismicity and tectonic relationships of the Nemaha Uplift in Oklahoma, Part III: U.S. Nuclear Regulatory Commission NUREG/CR-1500, 70 p.

Note: Sources in Parts IIa, IIIb, and IIIc include Kansas, Nebraska, and some Missouri earthquakes located by Don Steeples of the Kansas Geological Survey, and this information has also been published in U.S. Nuclear Regulatory Comission NUREG documents and other reports by the Kansas Geological Survey. Some Kansas and Nebraska earthquakes in sources IIIa, IIIb, and IIIc give both Oklahoma Geophysical Observatory and Kansas Geological Survey locations. When this has been the case, only the Oklahoma Geophysical Observatory location was entered in the Arcadia study data base. The two locations were never far enough apart to indicate any effect on seismic risk.

PART IV - Includes the three largest earthquakes of the 1811 and 1812 Mississippi Valley sequence.

Sources: IVa, Nuttli, O.W., 1973, The Mississippi Valley earth-quake of 1811 and 1812: intensities, ground motion and magnitudes: Bulletin of the Seismological Society of America, v. 63, p. 227-248.

The resulting data base consists of 428 earthquakes, which are listed chronologically in table 1 (Appendix). Table 1 also lists the distance of each epicenter from the Arcadia site in kilometers and the expected acceleration and velocity at the Arcadia site for each earthquake. The acceleration is computed from the following formulae of Nuttli and Herrmann (1978):

$$log(aH) = -0.36 + 0.52 \text{ mb}$$
  
 $R < 15 \text{ km}$   
 $log(aH) = -0.84 + 0.52 \text{ mb} - 1.02 log(R)$   
 $R > 15 \text{ km}$ , (1)

where aH = maximum horizontal acceleration of ground at site in cm/sec<sup>2</sup>, and R = great-circle distance from earthquake to site in km. The formulae have two forms, the first being applied for distances less than 15 km, and the second for distances of 15 km or greater. In the same publication, Nuttli and Herrmann gave a single formula for maximum horizontal ground velocity:

$$log(vH) = -2.92 + 1.0 \text{ mb} - 1.0 log(R).$$

Because this equation would allow vH to approach infinity as distance approached zero, the equation was converted to the following pair of formulae analogous to (1):

$$log(vH) = -4.10 + 1.0 \text{ mb}$$
  
 $R < 15 \text{ km}$   
 $log(vH) = -2.92 + 1.0 \text{ mb} - 1.0 log (R)$   
 $R > 15 \text{ km}$ , (2)

where vH = maximum horizontal ground velocity at site in cm/sec. All accelerations calculated from formula (1) were reduced to a percentage of g by dividing them by measured gravity at the Oklahoma Geophysical Observatory "rock gravity station" (U.S. Department of Defense catalog number 5279-1), and multiplying the quotient by 100. The "rock gravity station" has a measured gravitational acceleration of 979.720 cm/sec/sec.

Table 2 lists all of the earthquakes from table 1 which would have produced a horizontal acceleration of 0.1% g or greater at the Arcadia site. The listing is in order of acceleration. Only 10 earthquakes would have produced an acceleration of 1.0% g or more. They are the three large Mississippi Valley earthquakes of 1811-12, the 1952 El Reno earthquake and four of its aftershocks, the 1956 Edmond earthquake, and a 1939 Hughes County earthquake. The greatest site ground velocities listed were caused by the 1811-12 Mississippi Valley earthquakes.

#### OKLAHOMA SEISMIC-SOURCE ZONES

On the basis of the patterns of historical earthquakes and network earthquakes ("network earthquakes" refer to earthquakes located by arrival times at three or more network seismograph stations), Oklahoma and nearby areas were divided into six seismic-source zones. The zones were based on consistent patterns of earthquake occurrence. The zones do not appear to coincide with major geologic features, except that zone 2.2, southeast Oklahoma, contains most of the Ouachita front.

Table 2. Earthquakes from table 1 which would have produced a maximum horizontal ground acceleration of 0.1% g or more at the Arcadia site, listed in acceleration order. See table 1 for caption information.

YEAR	DATE	UTC	LAT DN	LON DW	ST	ММ	MAG	DELTAkm	Ah %g	Vh cm/sec
1812	FEB 7	0945	36.600	89.600	110	12	7.40	701.787	6.219690	43.032327
	APR 9	1629	35.400	97.800	OK	7		50.778	5.369235	2.596139
	DEC16	0815	36.600	89.600	МО	12		701.787	4.895181	27.151563
	FEB16	2330	35.700	97.500	OK	6	3.97	16.320	4.745926	0.687507
1812	JAN23		36.600	89.600	MO		7.10	701.787	4.342789	21.567253
	DEC 28	0030	35.500	98.000	OK	6	4.04	62.806	1.305377	0.209893
	APR16	0605	35.400	97.800	OK	5	3.85	50.778	1.291554	0.167621
	APR11	2030	35.400	97.800	OK	4	3.85	50.778	1.291554	0.167621
	APR16	0558	35.400	97.800	OK	F	3.85	50.778	1.291554	0.167621
1939	JUN 1		35.000	96.400	OK	4	4.37	111.021	1.083889	0.253860
1953	MAR17		35.400	98.000	OK	6	3.82	66.656	0.944015	0.119168
1937		1426	35.300	96.900	OK	4	3.61	55.015	0.892907	0.089026
1969	MAY 2		35.500	96.200	OK	F	4.08	103.480	0.822898	0.139683
1975	OCT12		35.500	97.700	OK		3.20	37.364	0.810952	0.050997
1959		1245	34.800	96.700	OK	5	3.97	110.414	0.675168	0.101619
1918	SEP11		35.500	98.000	OK	6	3.44	62.806	0.636409	0.052723
1918	SEP10	1630	35.500	98.000	OK	5	3.44	62.806	0.636409	0.052723
	OCT 22	2215	35.000	94.000	AR	7	4.80	310.419	0.635493	0.244372
1925	JUL30	1217	35.400	101.300	TX	5	4.92	360.102	0.630585	0.277699
1976	OCT 22	1715	35.380	97.060	OΚ		3.00	38.685	0.616041	0.031079
1867	APR24	2022	39.500	96.700	KS	7	5.05	431.391	0.612815	0.312701
1959	JUN17	1027	34.500	98.500	OK	6	4.22	166.284	0.599833	0.119991
1956	OCT30	1036	36.200	95.800	ΟK	7	4.12	150.629	0.588616	0.105218
1942	JUN12	0550	36.400	97.900	OK	3	3.70	97.824	0.552899	0.061597
1933	AUG19	1930	35.500	98.000	OK	5	3.31	62.806	0.544673	0.039084
1926	JUN 20	1420	35.600	94.900	OK	5	4.28	219.554	0.485428	0.104342
1956	JAN 6	1158	37.300	98.500	KS	б	4.20	211.057	0.459209	0.090282
1915	3 VOI	0000	36.200	95.800	OK	F	3.86	150.629	0.431153	0.057822
1975	NOV29	1429	34.650	97.530	OK	5	3.60	112.595	0.424961	0.042509
1976	NOV11	1612	35.850	97.320	OK		2.20	22.242	0.415699	0.00856 <b>7</b>
1961	APR27	0730	34.900	95.300	OK	5		202.134	0.415667	0.071509
1974	DEC16	0230	35.400	97.470	OK	3	2.42	30.529	0.391645	0.010358
1978	JUN16		32.961	100.794	TX	F	4.66	436.323	0.379746	0.125948
1919	JUL26			97.330	KS	5	4.09	225.572	0.376139	0.065572
			37.680			4		225.572	0.367238	
				101.300			4.45	358.520	0.360823	0.094512
			41.000	97.000		7	4.81	595.182	0.331097	
			35.630	98.408			3.25	97.375	0.324102	0.021956
			34.800	95.500			3.81	191.088	0.318595	0.040522
			35.502	9 <b>7.949</b>			2.74	58.311	0.296915	0.011330
				102.500			4.51	467.418	0.295800	0.083233
				100.700		5	4.17	317.060	0.292505	0.056036
			36.086	97.305			2.52	48.500	0.275321	0.003208
			36.070	97.506			2.50	49.288	0.264425	0.007714
1935	MAR 1	1100	40.300	96.200	ΝE	6	4.51	526.098	0.262186	0.073949

Table 2. (continued)

YEAR	DATE	UTC	LAT DN	LON DW	ST	MM	MAG	DELTAkm	Ah %g	Vh cm/sec
1939	JUN19	2143	34.100	93.100	AΡ	5	4.32	422.332	0.261295	0.059477
			34.200	95.600	OK	5	3.76	225.395	0.253568	0.030694
1966	JUL20			101.200	TX	5	4.13	349.374	0.252546	0.046420
1979	MAR18	2044		98.124	OK	3	2.85	77.873	0.252164	0.010930
1961	APR26	0705		95.000	OK	3	3.81	241.775	0.250621	0.032106
1929	SEP23	1100	39.000	96.600	KS	5	4.19	377.796	0.250551	0.049288
1918	OCT 4	0921	34.700	92.300	AR	5	4.37	468.903	0.249341	0.060106
1934	APR11	1740	33.900	95.500	OK	5	3.85	256.345	0.247683	0.033203
1975	OCT30		35.270	96.760	OK		2.70	66.667	0.246893	0.009038
1969	JAN 1	2336	34.800	92.600	AR	ΰ	4.30	439.619	0.244884	0.054566
1975	SEP13	0125	34.100	97.400	OK	5	3.40	172.353	0.216647	0.017522
1951	JUN20		35.500	103.000	ΥT	б	4.32	512.721	0.214397	0.048991
1927	JAN 7			97.680	KS	5	3.86	301.625	0.212345	0.028876
1968	OCT14		34.000	96.400	OK	6	3.50	202.021	0.207680	0.018819
1979	MAR14		35.519	97.781	OK	5	2.17	43.278	0.203380	0.004109
1906	JAN 8		39.300	96.600	KS	7	-	410.662	0.201718	0.035198
1978	JAN 8		35.824		OK		1.96	34.143	0.201432	0.003211
1979			35.923	97.480	OK	_	1.92	33.212	0.197503	0.003011
1929	OCT 21		39.200	96.500	KS	5		401.215	0.194560	0.032109
1911	_		33.800	92.200	AR	5	4.23	511.629	0.192914	0.039907
1941 1961	OCT18		35.400	99.000 94.600	OK	5 5	3.20	153.561	0.191819	0.012403
1979	DEC 25 SEP13		39.100 35.217	99.362	KS OK	4	4.11 3.37	452.858 190.162	0.189242 0.189057	0.034201 0.014821
1964	MAR28		42.900	101.600	NE	7	4.68	385.394	0.188981	0.064993
1978	FEB14		35.777	97.585	OK	,	1.69	26.990	0.185298	0.002182
			35.203	97.445	OK		2.22	50.750	0.183550	0.003932
1979			35.705	97.978	OK		2.34	58.809	0.182333	0.004473
,			35.343	97.997	OK	4		69.317	0.182322	0.005238
	MAY18		35.601	97.328	OK		2.11	45.309	0.180631	0.003418
1979			34.916	97.383	OK		2.61	81.703	0.180142	0.005995
1957	MAR19		32.000	95.000	TX	5		459.086	0.180039	0.031485
1978	MAY17	2311	35.525	97.910	ОК	1	2.26	54.221	0.179989	0.004035
1875	8 VOM	1040	39.300	95.500	KS	5	4.03	436.512	0.178526	0.029512
1979	SEP17	2041	35.320	97.968	OK	4	2.45	68.389	0.178326	0.004955
1979	MAR18	2142	35.394	98.108	OK		2.53	75.894	0.176476	0.005368
			35.870	99 <b>.</b> 9 <b>7</b> 0	OK	5	3.50	239.301	0.174733	0.015888
1977	OCT 6		35.820	97.767	OK		2.05	43.709	0.174386	0.003086
1904	OCT 27		37.700	100.000	ΚS	5	3.77	329.412	0.174262	0.021491
1978	SEP26		35.519	97.866	OK	_	2.15	50.578	0.169380	0.003358
	FEB15		34.000	93.000	AF	5	3.98	435.453	0.168569	0.026367
	MAR18		35.416	98.110	OK		2.48	75.173	0.167848	0.004330
	SEP27		35.519	97.843	OK OZ		2.10	48.591	0.166194	0.003115
	HAR19		35.400	98.110	OK OK	_	2.46	75.813	0.162466	0.004574
	MAR14 AUG14		34.000	95.000	OK		3.57 4.26	280.692	0.161474	0.015914
T 200	AUG14	1526	32.000	102.600	ΙΛ	6	4.20	633.373	0.160844	0.034541

Table 2. (continued)

YEAR	DATE	UTC	LAT DN	LON DW	ST	MM	MAG	DELTAkm	Λh %g	Vh cm/sec
			42.500		11E	5	4.41	761.306	0.159554	0.040592
			35.510	97.888	OK		2.12	52.773	0.156471	0.003003
	NOV10			96.800	OK		2.71	105.998	0.155702	0.005817
	APR16		· · · ·	99.970			3.40	239.301	0.155016	0.012620
	MAR27		35.300	101.200	ΥX	6	3.71	352.356	0.151418	0.017499
		0559		96.520	OK		2.34	73.469	0.145302	0.003580
	FEB 8	0010	37.400	92.400	МО	5	3.94	481.260	0.145101	0.021758
	MAR18		35.420		OK		2.34	75.019	0.142241	0.003506
			35.418	98.155			2.38	78.930	0.141681	0.003654
	APR28			97.201			1.83	41.550	0.141109	0.001956
			39.800		KS	5	3.96	509.687	0.140168	0.021513
			36.002	97.367			1.76	39.256	0.137505	0.001762
			35.427	97.717			1.83	42.878	0.136653	0.001896
1979			35.301	97.501			1.86	45.884	0.132192	0.001898
			35.455	97.905	OK		2.03	56.318	0.131474	0.002287
	MAR18		35.418		ОК		2.26	74.926	0.129412	0.002920
			35.449	97.927	OK		2.03	58.412	0.126667	0.002205
			35.498	97.826	OK		1.86	47.905	0.126506	0.001818
			39.000		KS		3.71	422.851	0.125715	0.014582
			34.920	95.730	OK	1	_	166.259	0.123508	0.005744
	MAY19			97.503	OK		2.02	59.333	0.123178	0.002122
1975			34.230	96.540	OK	_	2.91	173.424	0.119731	0.005635
1967			43.700	99.400	SD		4.32	911.859	0.119171	0.027547
1970			36.100	103.200	NH	6	3.85	530.892	0.117867	0.016032
			34.587		AR		3.39	314.933	0.115748	0.009371
			35.418	98.101			2.16	74.332	0.115745	0.002338
			34.672	97.157	OK	_	2.49	109.305	0.115415	0.003384
1934			42.700		ΝE	6	-	923.177	0.114897	0.025985
			35.606	95.296	OK		2.91	183.775	0.112857	0.005318
			35.200	95.800	OK		2.72	147.286	0.112661	0.004284
1979			35.429	97.871			1.87	54.735	0.111755	0.001628
1979			35.781	97.650	CK	_	1.42	32.333	0.111549	0.000978
1929			39.200	96.500	KS	כ	3.56	401.215	0.110829	0.010880
			35.683		OK		1.93	61.046	0.107430	0.001676
			35.187	97.664			1.90		0.106060	
			35.411		OK		2.14	79.872	0.105016	0.002078
			35.230		OK		2.30	97.851	0.103400	0.002452
			35.493	97.882	OK		1.77	52.854	0.102745	0.001339
			36.367	97.379	OK		2.12	79.794	0.102633	0.001986
			34.799	97.557	CK		2.28	96.781	0.102092	0.002367
	MAR12		34.994	96.625	OK		2.28	96.949	0.101912	0.002363
1979	MAR18	2340	35.433	98.102	OK		2.04	73.849	0.100922	0.001785

Zones are assigned descriptive names and, for convenience in computer use, were also assigned numbers. Zones with the most concentrated activity were numbered "1.X," where .X is a decimal fraction identifying the specific zone. Zones with less activity were numbered "2.X," and the remaining area was named "RESIDUAL," with a number of 3.1. Table 3 gives the source zone names, numbers, boundaries, and areas.

Figures 2a and 2b show a map of the zone boundaries, along with all earth-quakes known to have occurred through the end of 1979. The earthquake symbols are divided into two classes. An asterisk (\*) is used to denote earthquakes known to have been felt, whereas a plus (+) is used to denote earthquakes not known to have been felt (instrumentally located earthquakes). Most earthquakes prior to 1977 are known to have been felt. Because of poor seismograph-station coverage in this region, nearly all earthquakes prior to 1972 are only known because they were felt. The zones listed in table 3 occupy the entire area of the map except for the large rectangle excluded in the Texas Panhandle.

Because of uncertainty in locating epicenters, the older historical felt earthquakes tended to have identical coordinates listed for several different earthquakes, causing several earthquakes to be plotted as one symbol. To show more clearly the number of earthquakes, where two or more earthquakes are listed with exactly the same coordinates, they were spread slightly by having their symbols displaced by the following amount:

LATITUDE DISPLACEMENT = 0.09x degrees

LONGITUDE DISPLACEMENT = 0.06x degrees,

where x = a random number  $-0.5 \le x \le +0.5$ . The constants 0.09 and 0.06 in formula 3 were selected to spread the points just enought to be seen without moving them beyond their probable error of location. The difference in 0.09 and

Table 3. Seismic source zones of Oklahoma and surrounding areas.

Zone name	Zone number	Area (km <sup>2</sup> )	Boundaries (Given as latitude and longitude of each straight-line intersec- tion starting at the most north- easterly and proceeding clockwise)				
Central Oklahoma	1.1	1,232.4	35.55N 97.75W 35.25N 97.75W 35.25N 98.25W 35.55N 98.25W 35.55N 97.75W				
South-central Oklahoma	1.2	1,359.8	34.2 N 97.2 W 33.8 N 97.2 W 33.8 N 97.6 W 34.2 N 97.6 W 34.2 N 97.2 W				
North-central Oklahoma	2.1	4,232.8	36.4 N 97.0 W 36.1 N 97.0 W 35.55N 97.65W 35.55N 98.25W 36.4 N 97.4 W 36.4 N 97.0 W				
Southeast Oklahoma	2.2	32,668.9	35.55N 94.0 W 34.5 N 94.0 W 34.5 N 97.75W 35.55N 97.75W 35.55N 94.0 W				
West-central Oklahoma	2.3	12,292.7	36.0 N 98.5 W 35.0 N 98.5 W 35.0 N 100.0 W 36.0 N 100.0 W 36.0 N 98.5 W				
Residual	3.1	177,927.4	37.5 N 94.0 W 33.5 N 94.0 W 33.5 N 100.2 W 36.3 N 100.2 W 36.3 N 103.0 W 37.5 N 103.0 W 37.5 N 94.0 W Excluding area inside zone 1.1, 1.2, 2.1, 2.2, 2.3.				

0.06 reflects the difference in the length of 1 degree of latitude and 1 degree of longitude. At the equator, both are the same, but at 36°N latitude, 1 degree of latitude is 1.53 times greater (1/cos<sup>2</sup>(36°)) than 1 degree of longitude. It should be noted that the inclusion of a random number will cause maps printed at different times to vary in fine detail.

### MAGNITUDE-FREQUENCY RELATIONS IN OKLAHOMA SEISMIC-SOURCE ZONES

Magnitude was plotted against the cumulative frequency per year (the number of earthquakes of that magnitude or greater). Three different magnitudes, which were assumed to be nearly equivalent, were used. Where more than one magnitude was available for an earthquake, they were used in this order of preference:

- 1. mbLg of Nuttli (1973).
- 2. m3Hz of Nuttli (see Zollweg, 1974).
- 3. MDUR of Lawson (see Luza and Lawson, 1979).

For some of the earlier earthquakes for which the felt areas were known, mbLg was calculated using the formula developed by Nuttli and Zollweg (1974). Their formula was calibrated against six Oklahoma earthquakes and one Nebraska earthquake that occurred during 1974-78 (Luza and Lawson, 1980). Luza and Lawson (1980) included a table of 26 Oklahoma earthquakes (table 4, p. 59) for which magnitude was calculated from area. Of particular interest is the resulting 5.04 magnitude for the 1952 El Reno earthquake. This earthquake has been rated at magnitude 5.5 on the basis of one P-wave amplitude recorded at Pasadena, California. Also of importance to the Arcadia study is the 3.97 magnitude of the 1956 Edmond earthquake, calculated from its felt area of 12,950 km<sup>2</sup>.

Figure 3 shows the log cumulative frequency vs. magnitude plot for zone 1.1, central Oklahoma. Network-located earthquakes of magnitude 2.0 to 3.0 were assumed to be complete for 3 years (1977-79 inclusive). Historical earthquakes with magnitudes between 3.0 to 4.0 were assumed complete from 1900 to 1976

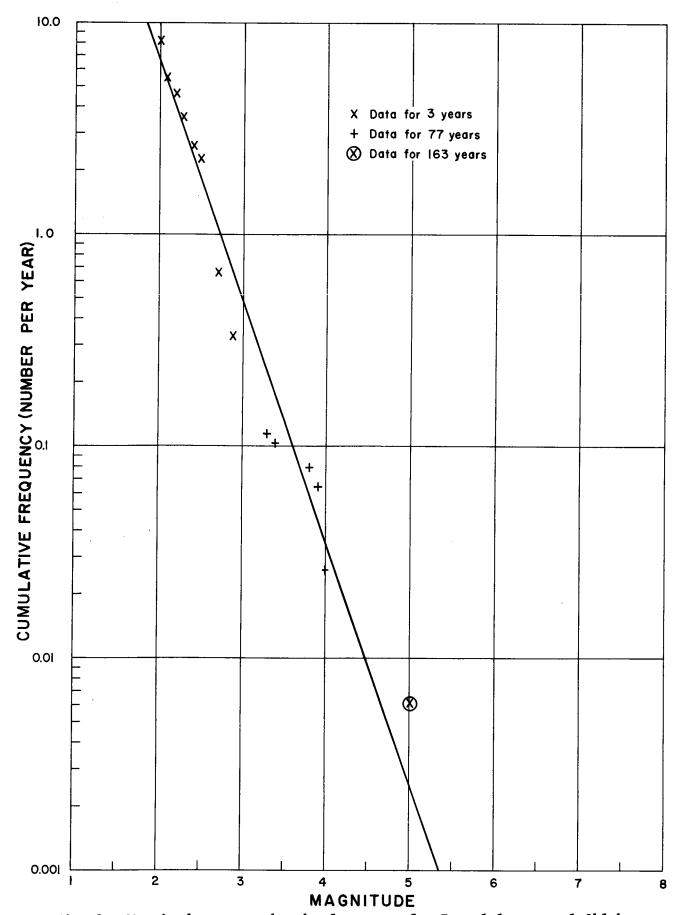


Fig. 3. Magnitude vs. earthquake frequency for Zone 1.1, central Oklahoma.

inclusive, a period of 77 years. Dr. Bob Fay (Oklahoma Geological Survey, personal communication) is fairly certain that no earthquake as large as the 1952 El Reno earthquake could have occurred in the past 163 years without having been documented; thus that earthquake is plotted with a frequency of 1/163.

The network and the historical earthquakes in figure 3 fit a straight line fairly well. Using all the points with equal weight, with methods given by Lapin (1975), a least-squares line was calculated (see table 4). Student's T 95% confidence limits on the constants were calculated by the method of Hyans and Philpot (1971).

Similar graphs and calculations were made for the other seismic zones (table 4). South-central Oklahoma (zone 1.2) is omitted from the table because preliminary calculations gave an apparently anomalous least-squares line. This zone should not be important to the Arcadia study. The Texas Panhandle area was excluded from the residual areas (see fig. 2a) because it appears anomalous whether combined with the residual area, combined with the west-central Oklahoma area, or taken by itself.

Except for central Oklahoma (zone 1.1) and south-central Oklahoma (zone 1.2), the frequencies in the other zones were divided by their areas in 1,000-km<sup>2</sup> units and the lines recalculated. This procedure was suggested by Professors Otto Nuttli and Robert Herrmann (1978) to equalize frequencies in large source zones.

Most magnitude vs. log-frequency calculations give log frequency as a function of magnitude:

$$\log(N) = a + bm. \tag{4}$$

This study gives magnitude as a function of frequency:

$$m = A + B \log(N). \tag{5}$$

The lines given by (4) and (5) cannot be converted from one form to the other by simple algebraic manipulation. The least-squares fitting procedure calculates a

Table 4. Equations estimating largest magnitude (M) that will occur with frequency of  $\underline{f}$  per year per 1,000 km<sup>2</sup> of source zone. (For zone 1.1, frequency is f per year for entire zone, which is 1,232 km<sup>2</sup> in area. Numbers following  $\pm$  indicate 95% confidence limits.)

```
Zone 1.1 Central Oklahoma
    M = 2.7241 ± 0.049893 -(0.87951 ± 0.048971) log(f)
Zone 2.1 North-central Oklahoma
    M = 1.8241 ± 0.019184 -(0.86024 ± 0.018579) log(f)
Zone 2.2 Southeast Oklahoma
    M = 1.1716 ± 0.052239 -(0.99229 ± 0.026765) log(f)
Zone 2.3 West-central Oklahoma
    M = 1.5062 ± 0.21077 -(0.72025 ± 0.090866) log(f)
Zone 3.1 Residual
    M = -0.27607 ± 0.13897 -(1.2692 ± 0.057652) log(f)
```

slightly different line for (4) and (5). The relationship in formula (5) is preferred in this study because it gives the magnitude of the largest earthquake to be expected in any source zone for any given time interval. Table 4 gives the equations in formula (5) for all zones except 1.2, south-central Oklahoma. In table 4, the equation for the largest magnitude expected in the entire zone with an earthquake frequency of f per year may be obtained by adding the following number to the right-hand side of the equation:

 $\log(\text{zone area in km}^2/1,000)$ .

This does not apply to zone 1.1 because the equation represents the entire zone.

The largest magnitude earthquake expected in each 1,000  $\mathrm{km}^2$  of a zone in a period of P years is determined by substituting 1/P for f in the appropriate equation and calculating M. This procedure was used to produce table 5, giving the largest earthquake expected for the entire zone and for each 1,000  $\mathrm{km}^2$  of the zone for various periods.

ASSESSMENT OF MAXIMUM HORIZONTAL GROUND VELOCITY AND HORIZONTAL GROUND ACCELERATION EXPECTED AT ARCADIA DAM SITE FROM EARTHQUAKES

For each seismic-source zone, a maximum expected earthquake magnitude for a given period was taken from table 5. This earthquake was assumed to occur at about 900 to 1,000 points of a square grid evenly and completely filling the source zone. The distance to the Arcadia dam site for each grid point was calculated, after which formulae (1) and (2) were used to calculate the aH and vH caused by the hypothetical earthquake. Approximately 900 to 1,000 values of aH and vH were stored in arrays. For aH, the largest one-tenth of the values were sorted and their arithmetic mean taken. The same sorting and averaging procedures were then done for vH. The resulting average aH and vH values were listed as the aH and vH expected at the site during the given time period from earthquakes within the

Table 5. Largest-magnitude earthquake expected in entire seismic zone (part a), and in each 1,000  $\rm km^2$  of each zone (part b), for various periods.

		(a) E	ntire zoı	nes								
Zone	Zone Period in years											
	100	200	500	1000	2000							
1.1	4.48	4.75	5.10	5.36	5.63							
2.1	4.08	4.34	4.68	4.94	5.20							
2.2		4.96										
2.3	3.65	3.86		4.37								
3.1	5.01			6.22	6.58							
	(b) Each 1,000 km <sup>2</sup> of zone, except entire zone 1.1											
		Perio	d in year	s								
Zone	_100	200	500	1000	2000							
1.1	4.48	4.75	5.10	5.36	5.63							
2.1	3.54	3.80	4.15	4.40	4.66							
2.2	3.16			4.15	4.45							
2.3	2.95			3.67	3.88							
3.1	2.26	2.64	3.15	3.53	3.91							
		*			- · • <del>-</del>							

source zone being studied. The values of the expected aH and vH,together with the expected maximum magnitude from table 5, were used with formulae (1) and (2) to calculate the "equivalent distance" at which the maximum-magnitude earthquake would have to occur to produce the given motion. Using this equivalent distance and the maximum magnitude (from table 5), the following equations of Nuttli and Herrmann (1978) were used to calculate an equivalent Modified Mercalli intensity at the site:

$$I = -3.5 + 2 \text{ mb}$$

$$R < 20 \text{ km}$$

$$I = -0.4 + 2 \text{ mb} -2.46 \log(R)$$

$$R > 20 \text{ km},$$
(6)

where I = equivalent Modified Mercalli intensity at the site, and R = great-circle distance from earthquake site to km. In common with formulae (1) and (2), this has two forms. The near-field form, or distances less than 20 km, simply gives a constant value dependent only on magnitude. The second form, for distances of 20 km or more, attenuates the intensity with distance. As with formulae (1) and (2), when R approaches zero, I will approach infinity; therefore, two separate forms, near field and far field, were used to avoid this situation.

The Modified Mercalli intensity scale was defined in 12 discrete steps. However, because it is common to assign in-between values—i.e., MM III—IV—the decimal fractions produced by formula (6) are not inconsistent with the MM intensity scale. A more serious problem occurs when formula (6) produces a number greater than 12 (mb 7.75 in the near field). Because the MM scale defines 12 as "damage total," any number greater than 12 could be simply considered 12. Any intensity number less than 1.0 could be simply considered not felt. The lower cutoff is not strictly accurate, because a 1.6-magnitude earthquake was felt in Love County, Oklahoma (Lawson and DuBois, 1976), and an earthquake as small as 0.8 magnitude was felt in Glenalmond, Scotland (Crampin and others, 1972).

Earthquakes of less than 2.25 magnitude would be below MM intensity 1.0 in the near field.

Values for aH and vH were calculated separately. Because aH attenuates as -1.02 log(R) and vH attenuates as -1.00 log(R), for some site source-zone geometries the equivalent distances could be different. However, this difference was found to be in no case greater than 0.4%, so it was ignored and the equivalent distance for aH was listed.

The calculations were done separately for each seismic source zone, and only the zone giving the largest values of aH and vH was used in the final assessment. As an example, consider the calculation of site aH and vH expected in 2000 years from earthquakes in seismic source zone 1.1. From table 5 (which came in turn from the least-squaresline in fig. 3), the maximum expected earthquake in 2000 years would have a magnitude of 5.63. It is assumed to occur at each point of a square grid that uniformly fills the entire zone with 930 points. The grid spacing is 1.17 km (0.0105 degrees of latitude and 0.0159 degrees of longitude). When site accelerations from magnitude-5.63 earthquakes are calculated for each point, the resulting accelerations vary from 14.0% g to 0.583% g. The average of all 930 points is only 7.78% g, but the average of the 93 largest values of aH is 12.0% g, which is the figure used. From formula (1), a 12.0% acceleration would be produced by a magnitude-5.63 earthquake if it were 46.0 km away from the site. The figure 46.0 km is the equivalent distance. From formula (6), a magnitude-5.63 earthquake at a distance of 46.0 km produces an equivalent site intensity of 6.77. The calculations for vH gave 11.2 cm/sec.

Because zone 1.1 gave higher aH and vH than any other zone, we would assess the 2000-year strongest ground motion as:

aH = 12.0% vH = 11.2 cm/sec (which is equivalent to a magnitude-5.63 earthquake at a distance of 46.0 km, and which is also equivalent to an MM intensity of 6.32 at the site). Table 6 lists the parameters of the largest expected ground motion at Arcadia dam site for six different time periods. For reference, table 7 lists the acceleration expected from each zone for different periods. For reasons mentioned previously, zone 1.2 is omitted. However, calculations show that for any given period, an earthquake in zone 1.2 would necessarily exceed magnitude 6.7 to produce a greater acceleration than earthquakes in zone 1.1. An earthquake exceeding magnitude 6.1 in zone 1.2 would be necessary to produce a greater site velocity than that produced by earthquakes in zone 1.1. Although a stable least-squares line relating log frequency to magnitude in zone 1.2 has not yet been determined, there is nothing to suggest that earthquakes of magnitude 6.1, and particularly 6.7, could be expected to occur there in periods of 2000 years or less.

#### COMPARISON WITH HISTORICAL GROUND MOTION

Table 2 indicates an aH of 6.2% g and a vH of 43.0 cm/sec for the Arcadia dam site from the Feb. 7, 1812, Mississippi Valley earthquake. Nuttli and Herrmann (1978) considered this the maximum-magnitude earthquake that could occur in the Mississippi Valley. The 1952 El Reno earthquake produced an aH of 5.4% g and a vH of 2.6 cm/sec and probably had a Modified Mercalli intensity of 4.5 to 5.5 at the site (unpublished study of newspaper reports). Except for vH, these parameters are consistent with ground motion projected for 500 years or less in table 6.

#### DISCUSSION OF ASSUMPTIONS USED IN ARCADIA STUDY

The overall assumption in the study is that future seismicity, for as long as 2000 years, will follow the spatial and temporal patterns of the last 70 years. This assumption should be rated fair to poor. The July 27, 1980, earthquake

Table 6. Largest expected earthquake magnitude, equivalent distance, site intensity, and site aH and vH at Arcadia site for various periods.

Period (years)	Largest magnitude	Equivalent distance (km)	Equivalent site intensity (MM)	Site aH (% of g)	Site vH (cm/sec)
100	4.48	46.0	4.47	3.04	0.790
200	4.75	46.0	5.01	4.20	1.47
500	5.10	46.0	5.71	6.38	3.29
1000	5.36	46.0	6.23	8.71	5.99
2000	5.63	46.0	6.77	12.0	11.2

Table 7. Acceleration values, aH, in percent g, expected at Arcadia site for each seismic-source zone (except for 1.2) for various periods.

Period			Zon	e	
(years)	1.1	2.1	2.2	2.3	3.1
100	3.04	2.36	0.796	0.192	0.131
200	4.20	3.22	1.13	0.246	0.207
500	6.38	4.89	1.82	0.349	0.381
1000	8.71	6.60	2.60	0.454	0.600
2000	12.0	9.01	3.73	0.583	0.946

northeast of Lexington, Kentucky, having a magnitude of 5.3 (Oklahoma Geophysical Observatory, mbLg), occurred in an area essentially free of historical seismicity. The method used in this study would have assigned extremely low risk to this area. However, the 1952 earthquake at El Reno, Oklahoma, having a magnitude of 5.0, was preceded by earthquakes (as early as 1908) and followed by earthquakes (as late as 1980). In more active seismic areas of the world, particularly at lithospheric plate boundaries, causative geological structures might be identifiable but even in such cases past seismicity is relied upon to define which of these structures may be active.

A discussion of detailed assumptions follows:

- 1. Seismicity in Oklahoma is confined to fairly well-defined source zones and is reasonably homogeneous within those zones. The assumption is fair to good in describing seismicity to date, especially in the light of the close agreement between historical felt earthquakes and network-located earthquakes. As noted above, the assumption is fair to poor when extended to long periods in the future.
- 2. Seismicity follows the formulae in table 4. This assumption is good. Note that if the 1952 El Reno earthquake were removed from figure 3, the least-squares line would be almost unchanged. In effect, if the El Reno earthquake had not occurred until after this study, it would have been accounted for by the least-squares line. This assumption is only fair when projected far into the future.
- 3. Attenuation relations (1), (2), and (6) are correct. This assumption is good. Nuttli and Herrmann based the formulae on much Mississippi Valley and other data. Oklahoma appears to have the same attenuation characteristics.

- 4. The three magnitudes used are equivalent. This assumption is very good.
- 5. When estimated from felt areas using Nuttli and Zollweg's (1974) relation, mbLg is equivalent to mbLg calculated from seismograph—measured LgZ waves. This assumption is very good. The relations have been checked against all Oklahoma earthquakes with both accurately measured LgZ waves and well-defined felt areas.
- 6. Assessed risk is not a strong function of grid spacing within the source zones. This is a good assumption. The 2000-year aH value for Arcadia was 12.0% g with 1.17-km grid spacing in zone 1.1, 12.2% g with 2.34-km spacing, and 12.5% g with 4.67-km spacing.
- 7. It is reasonable to average ground motion produced by earthquakes at grid points accounting for only the largest 10% of the aH values. This assumption is an arbitrary deterministic element. If earthquakes are, as assumed, equally likely to occur anywhere within a source zone, this assumption could be accounted for by stating that the aH (or vH or I) for a given period had about a 95% probability of not being exceeded.

# DISCUSSION OF RESULTS

Table 6 gives a list of maximum horizontal ground acceleration, maximum horizontal ground velocity, and equivalent Modified Mercalli intensity to be expected at the Arcadia dam site for various time periods. The aH, vH, and intensity between the tabulated values may be obtained by log log interpolation. For graphical interpolation, plot aH (or vH or intensity) on the horizontal axis of log log paper, and the frequency in number per year (1/period in years) on the vertical axis. It probably would not be useful to extrapolate the values outside the table values. The maximum magnitude of earthquakes expected for periods between the

tabulated values may be obtained by log linear interpolation (as in fig. 3) or from the first equation in table 4, keeping in mind that for each given period the maximum ground-motion parameters were due to earthquakes in seismic-source zone 1.1, central Oklahoma.

The different values for the ground-motion parameters are intended to be a guide for the construction engineer, who can select the appropriate interval to satisfy one or more of the following conditions: (1) structure to remain completely undamaged, (2) structure to be damaged only slightly, and (3) structure to sustain severe damage but catastrophic failure to be avoided. Having selected one or more time intervals, table 6 (with interpolation if necessary) may be used to determine the relevant ground-motion parameters. Except as noted below, very little arbitrary conservatism has been built into the results in table 6. The design may be made more conservative by extending the period used in determining the ground-motion parameters beyond the expected life of the structure, but only the design engineer should decide whether or not to make any extension, and how large the extension should be. It is also possible that for non-critical substructures, tradeoffs in cost and other factors may make it desirable to decrease the period used in determining ground motion to something less than the life of the structure.

The method used in this study is both probabilistic and deterministic. It is probabilistic in defining source zones and determining the largest earthquake expected in the source zones in any given period. It is deterministic in that it averages the ground motion from only the 10% of grid points within the zone that would produce the largest ground motion at the site. This averaging the largest 10% is an almost arbitrary conservatism. In the case of the Arcadia 2000-year risk, had all the grid points in zone 1.1 been averaged, the value of aH would have been 7.87% instead of the 12% given in table 6.

The earthquakes that occurred at or very near the Arcadia dam site were not ignored. In zone 3.1, some grid points were at and very near the site. Nuttli and Herrmann's (1978) equations limit the near-field (nearer than 15 km) ground motion. The limit is very realistic. If the equations contained a term in minus log(R) for all distances, aH and vH would approach infinity as the distance to the site approached zero.

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APPENDIX

Earthquake List

Table 1. List of 428 earthquakes, January 1, 1800, to December 31, 1979, used in the Arcadia study.

YEAR	DATE	UTC	LAT DN	LON DW	ST	MM	MAG	DELTAkm	Ah %g	Vh cm/sec
1811	DEC16	0815	36.600	89.600	мо	12	7.20	701.787	4.895181	27.151563
	JAN23		36.600	89.600	MO	12	7.10	701.787	4.342789	21.567253
1812	FEB 7	0945	36.600	89.600	МО	12		701.787	6.219690	43.032327
1867	APR24		39.500	96.700	KS	7	5.05	431.391	0.612815	0.312701
			42.700	97.000	NE	5	3.80	783.905	0.074602	0.009677
		1040	39.300	95.500	KS	5	4.03	436.512	0.178526	0.029512
1877		1745		97.000	NE	F		595.182	0.000000	0.000000
1877		1830		97.000	NE	7	4.81	595.182	0.331097	0.130422
1882	OCT22	2215	35.000	94.000	AR	7	4.80	310.419	0.635493	0.244372
1895	OCT11	2355		103.300	SD	5		1048.973	0.046315	0.005120 0.005120
1895	OCT12	0125		103.300	SD	5	3.65		0.046315 0.000000	0.003120
1900	DEC 0	0000	36.000	96.800	OK OK	4 F		61.585 61.585	0.000000	0.000000
	APR 1		36.000	96.800 96.800	OK	F		61.585	0.000000	0.000000
1901		1330 1800	36.000 42.500	97.500	NE	5	4.41	761.306	0.159554	0.040592
	OCT27	2359	37.700	100.000	KS	5	3.77	329.412	0.174262	0.021491
1904	JAN 8	0015	39.300	96.600	KS	7	4.08	410.662	0.201718	0.035198
	MAY10	0027	43.000	101.300	NE	6	4.03	885.151	0.086804	0.014554
1908	JUL19	0000	35.700	97.700	OK	3	4.03	33.857	0.000000	0.000000
1909	JAN 26	2015		97.767	NE	5	3.56	745.453	0.058915	0.005856
1910	0	0000	35.500	98.000	OK	F	3.30	62.806	0.000000	0.000000
1910	FEB26	0800	41.433	97.383	NE	5		642.618	0.000000	0.000000
1911	MAR31	1657	33.800	92.200	AR	5	4.23	511.629	0.192914	0.039907
1915	OCT 23	0605	43.800	101.500	SD	5		973.220	0.000000	0.000000
1915	8 VOII	0000	36.200	95.800	OK	F	3.86	150.629	0.431153	0.057822
1917	MAR27	1956	35.300	101.200	TX	6	3.71	352.356	0.151418	0.017499
1918	0	0000	35.500	97.700	OK	4		37.364	0.000000	0.000000
1918	SEP10	1630	35.500	98.000	OK	5	3.44	62.806	0.636409	0.052723
1918	SEP11		35.500	98.000	СK	6	3.44	62.806	0.636409	0.052723
1918	SEPll		35.500	98.000	OK	6		62.806	0.000000	0.000000
1918	OCT 4	0921	34.700	92.300	AR	5	4.37	468.903	0.249341	0.060106
1919	MAY27	0400	37.680	97.330	KS	4	4.07	225.572	0.367238	0.062620
1919	JUL26		37.680	97.330	KS	5	4.09	225.572	0.376139	0.065572
1924	JUN 3		36.300	96.500	OK	3	4 00	103.864	0.000000	0.000000
1925				101.300		5	4.92	360.102	0.630585	0.277699
1926		0000			KS	F	4 20	528.471	0.000000	0.000000
1926	JUN 20	1420		94.900	OK	5	4.28	219.554	0.485428	0.104342 0.028876
1927	JAN 7	0930	38.350	97.680	KS	5	3.86	301.625 515.161	0.212345 0.065210	0.004989
1927 1928	MAR18 NOV16	1725	40.000	95.300 103.700	KS SD	5 5	3.33 3.71	1075.366	0.048519	0.005734
1928	SEP23	1000	39.000	96.600	KS	F	3 • /I	377.796	0.000000	0.000000
1929	SEP23	1100	39.000	96.600		5	4.19	377.796	0.250551	0.049288
1929	OCT 21			96.500	KS	5	4.03	401.215	0.194560	0.032109
1929			37.180			4		276.605	0.000000	0.000000
1929	DEC 7		39.200	96.500			3.56	401.215	0.110829	0.010880
			22.200	22,000		_		· ·		

Table 1. (continued)

YEAR	DATE	UTC	LAT DN	LON DW	ST	MM	MAG	DELTAkm	Ah %g	Vh cm/sec
1020	DEC28	0030	35.500	98.000	O.K.	6	4.04	62.806	1 205277	
	AUG 9		39.100	94.700		6	3.33	448.219	1.305377 0.075158	0.209893 0.005735
	JAN29		39.000	99.600		6	3.71	422.851	0.125715	0.003733
	FEB20	1700	39.800	99.800		5	3.96	509.687	0.140168	0.021513
	AUG 8	0000	41.867	103.667		5		882.469	0.000000	0.000000
1933	AUG19	1930	35.500	98.000		5	3.31	62.806	0.544673	0.039084
	APR11		33.900	95.500		5	3.85	256.345	0.247683	0.033203
	JUL30	0720	42.700	103.000		6	4.30	923.177	0.114897	0.025985
	MAR 1	1100	40.300	96.200		6	4.51	526.098	0.262186	0.073949
	NOV 29		36.200	97.000		F		67.947	0.000000	0.000000
1936	MAR14		34.000	95.000		5	3.57	280.692	0.161474	0.015914
1936	JUN20		35.800	101.300		5	4.45	358.520	0.360823	0.094512
1936			36.900 35.300	103.000		F	3.31	526.583	0.062259	0.004662
1937 1938	OCT11		43.550	96.900 96.720		4 5	3.61 3.80	55.015 879.392	0.892907 0.066349	0.089026
1939	JUN 1		35.000	96.400		4	4.37	111.021	1.083889	0.008626 0.253860
1939	JUN19	2143	34.100	93.100		5	4.32	422.332	0.261295	0.059477
1941			35.400	99.000		5	3.20	153.561	0.191819	0.012408
1942	JUN12		36.400	97.900	OK	3	3.70	97.824	0.552899	0.061597
1942		1000	38.850	99.330		5		397.155	0.000000	0.000000
1948			36.000	102.500	ΤX	6	4.51	467.418	0.295800	0.083233
1948	APR 2		37.700	97.330	KS	4		227.794	0.000000	0.000000
1950	FEB 8		37.400	92.400	MO	5	3.94	481.260	0.145101	0.021758
1951		1937	35.500	103.000	ΤX	6	4.32	512.721	0.214397	0.048991
	APR 9	1629	35.400	97.800	OK	7	5.04	50.778	5.369235	2.596139
	APR 9		35.400	97.800	OK	F	2 05	50.778	0.000000	0.000000
	APR11 APR16	0558	35.400	97.800	OK	4	3.85	50.778	1.291554	0.167621
1952	APRIO	0605	35.400 35.400	97.800 97.800	OK OK	F 5	3.85 3.85	50.778 50.778	1.291554 1.291554	0.167621 0.167621
1952			35.400	97.800		F	3.03	50.778	0.000000	0.000000
	MAY 2		35.400	97.800		F		50.778	0.000000	0.000000
1952	JUN16			97.800	OK	F		50.778	0.000000	0.000000
1952	JUN16			97.800	OK	F		50.778	0.000000	0.000000
1952	JUN16	0000	35.400	97.800	OK	F		50.778	0.000000	0.000000
1952	JUN16	0000	35.400	97.800	OK	$\mathbf{F}$		50.778	0.000000	0.000000
			35.400	97.800	OK	F		50.778	0.000000	0.000000
1952			35.400	97.800	OK	F		50.778	0.000000	0.000000
1952			35.400	97.800	OK	4		50.778	0.000000	0.000000
1952	JUL17		35.400	97.800	OK	F		50.778	0.000000	0.000000
	AUG14		35.400	97.800	OK	4		50.778	0.000000	0.000000
	OCT 8	0415	35.100	96.500	OK	4		96.904	0.000000	0.000000
	MAR16		35.400	97.800 98.000	OK	3		50.778	0.000000	0.000000
	MAR17		35.400 35.400	98.000	OK OK	5 6	3.82	66.656	0.000000	0.000000
			34.800	96.700	OK	4	J. 02	66.656 110.414	0.944015	0.119168
TANA	2014 0	T / 4 U	74.000	30.700	OK	4		TT0.4T4	0.00000	0.000000

Table 1. (continued)

YEAR	DATE	UTC	LAT DN	LON DW	ST	MM	MAG	DELTAkm	Ah %g	Vh cm/sec
1954	APR 0	0000	35.100	96.400	ОК	4		104.092	0.000000	0.000000
1954	APR11		35.100	96.400	OK	4		104.092	0.000000	0.000000
1954	APR12	2305	35.100	96.400	OK	4		104.092	0.000000	0.000000
1954	APR13	1848	35.100	96.400	OK	4		104.092	0.000000	0.000000
1956	JAN 6	1158	37.300	98.500	KS	6	4.20	211.057	0.459209	0.090282
1956	FEB16	2330	35.700	97.500	OK	6	3.97	16.320	4.745926	0.687507
1956	APR 2	1603	34.200	95.600	OK	5	3.76	225.395	0.253568	0.030694
1956	OCT30	1036	36.200	95.800	OK	7	4.12	150.629	0.588616	0.105218
1957	MAR19	0016	32.000	95.000	TX	5	4.08	459.086	0.180039	0.031485
1959	JUN15	1245	34.800	96.700	OK	5	3.97	110.414	0.675168	0.101619
1959	JUN17	1027	34.500	98.500	OK	6	4.22	166.284	0.599833	0.119991
1960	MAR18	2130	36.200	95.800	OK	F		150.629	0.000000	0.000000
1960	MAR18	2330	36.200	95.800	OK	F		150.629	0.000000	0.000000
1961	JAN11	0140	34.800	95.500	OK	5	3.81	191.088	0.318595	0.040622
1961	APR13	2115	39.900	100.000	KS	5	3.63	527.276	0.091205	0.009727
1961	APR26	0705	34.600	95.000	OK	3	3.81	241.775	0.250621	0.032106
1961	APR27	0300	34.600	95.000	OK	F		241.775	0.000000	0.000000
1961	APR27	0500	34.600	95.000	OK	F		241.775	0.000000	0.000000
1961	APR27	0730	34.900	95.300	OK	5	4.08	202.134	0.415667	0.071509
1961	DEC 25	1220	39.100	94.600	KS	4		452.858	0.000000	0.000000
1961		1258	39.100	94.600	KS	5	4.11	452.858	0.189242	0.034201
	APR28		35.300	98.600	OK			121.327	0.000000	0.000000
	MAY18	0240	35.100	95.400	OK			185.238	0.000000	0.000000
	AUG 4	0018	35.200	95.600	OK			164.435	0.000000	0.000000
1962	SEP 1		35.200	96.000	OK			130.397	0.000000	0.000000
	JAN15		34.600	95.900	OK			174.653	0.000000	0.000000
1963	MAR13		34.600	95.900	OK			174.653	0.000000	0.000000
1963	JUN12	1208	34.700	96.800	OK			116.021	0.000000	0.000000
1963	JUN12	1638	34.700	96.800	OK			116.021	0.000000	0.000000
1963	JUL14	8080	35.000	97.700	OK			79.637	0.000000	0.000000
1963	JUL14	0810	35.000	97.700	OK	_		79.637	0.000000	0.000000
1964 1964	FEB 2 MAR24	0822 0612	35.100	99.100	OK	5	2 (5	171.620	0.000000	0.000000
1964		1009	43.500 42.900	103.500	SD NE	5 <b>7</b>	3.65	1019.876	0.047663	0.005266
			35.700	101.600		′	4.68	885.394	0.188981	0.064993
						=	2.30		0.048635	0.001170
	AUG14			101.200		6	4.13 4.26	349.374 633.373	0.252546	0.046420
			43.700	99.400	SD	5	4.32		0.160844	0.034541
			34.850	95.550	OK	4	7.52	911.859 184.371	0.119171 0.000000	0.027547 0.000000
			34.000	96.400	OK	F	2.30	202.021	0.049362	0.0001187
	OCT11		34.000	96.400	OK	F	1.93	202.021	0.031695	0.0001187
			34.000	96.400	OK	F	2.80	202.021	0.089824	0.003755
	OCT11		34.000	96.400	OK	F	2.40	202.021	0.055641	0.001495
			34.000	96.400	OK	-	2.00	202.021	0.034466	0.000595
			34.000	96.400	OK		1.80	202.021	0.027127	0.000375
		5550	5.,000	500100	~11		~ • • • •		0.02/12/	0.000373

Table 1. (continued)

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YEAR	DATE	UTC	LAT DN	LON DW	ST	MM	MAG	DELTAkm	Ah %g	Vh cm/sec
1060										
			34.000	96.400	OK		1.80	202.021	0.027127	0.000375
	OCT12		-	96.400	OK		2.60	202.021	0.070696	0.002369
	OCT14			96.400	OK		2.00	202.021	0.034466	0.000595
	OCT14			96.400	OK			202.021	0.000000	0.000000
	OCT14			96.400	OK	6	3.50	202.021	0.207680	0.018819
1968		0719	34.000	96.400	OK		1.70	202.021	0.024065	0.000298
	OCT17			96.400	OK		2.00	202.021	0.034466	0.000595
1968	OCT18	2114		96.400	OK		2.80	202.021	0.089824	0.003755
1968	NOV15	1041	34.000	96.800	OK		2.60	189.613	0.075418	0.002524
1969	JAN 1	2336	34.800	92.600	AR	6	4.30	439.619	0.244884	0.054566
1969	MAY 2	1133	35.500	96.200	OK	F	4.08	103.480	0.822898	0.139683
1969	MAY 2	1154	35.500	96.200	OK			103.480	0.000000	0.000000
1970			36.100	103.200	NM	6	3.85	530.892	0.117867	0.016032
1971	MAR 1			94.900	OK	_		228.493	0.000000	0.000000
1971	MAR13			95.800	OK		2.72	147.286	0.112661	0.004284
1972	OCT16			99.600	NE	5		764.518	0.000000	0.000000
1973	JAN10			98.000	OK	1	2.28	102.815	0.095984	0.002228
1973	SEP28			94.900	OK	_	2.00	252.542	0.027448	0.000476
1973			35.800	95.200	OK		1.92	192.868	0.032835	0.000518
1973			36.800	97.000	OK		1.94	131.166	0.049833	0.000798
1973	NOV18		35.000	94.700	OK		2.48	249.136	0.049446	0.001457
1973	DEC25		35.100	94.500	OK		2.80	263.593	0.068477	0.001437
1974				97.030	OK		2.18	130.586	0.066724	0.001393
1974		1334		100.700	ΤX	5		317.060	0.292505	0.056086
1974			34.000	93.000	AR	5	3.98	435.453	0.168569	0.026367
1974	MAY10	0115	34.200	97.300	OK	,	2.60	161.146	0.089030	0.002970
1974			34.800	96.800	OK		2.71	105.998	0.155702	
	DEC16		35.400	97.470	OK	3	2.42	30.529	0.391645	0.005817
	MAR31		35.606	95.296	OK	5	2.91	183.775		0.010358
	MAY13			98.400	NE	6	4.71		0.112857	0.005318
1975	MAY25		35.000			O	2 00	722.670	0.000000	0.000000
1975	JUN16		34.230	96.380	OK		2.00	112.404	0.062676	0.001070
1975	SEP13		34.230	96.540	OK	=	2.91	173.424	0.119731	0.005635
1975			35.500	97.400	OK	Э	3.40	172.353	0.216647	0.017522
				97.700	OK		3.20	37.364	0.810952	0.050997
			35.270	96.760		_	2.70	66.667	0.246893	
			34.650	97.530			3.60	112.595	0.424961	0.042509
			34.100	97.400			2.50	172.353	0.073748	0.002206
			35.900	92.100		5		472.318	0.000000	0.000000
			35.540	95.420			2.06	173.013	0.043377	0.000798
			35.590	96.520			2.34	73.469	0.145302	0.003580
			35.430	95.600			2.68	158.323	0.099762	0.003635
				102.250		5	2.10	455.965	0.016935	0.000332
				102.250			2.70	455.965	0.034737	0.001322
			35.870	99.970	OK	4	3.40	239.301	0.155016	0.012620
1976	APR17	0248	34.100	97.400	OK	2	2.40	172.353	0.065426	0.001752

Table 1. (continued)

YEAR	DATE	UTC	LAT DN	LON DW	ST	MM	MAG	DELTAkm	Ah %g	Vh cm/sec
1976	APR19	0442	35.870	99.970	ОК	5	3.50	239.301	0.174733	0.015888
1976	JUN 7	0130	34.660	94.620	OK		1.90	269.664	0.022775	0.000354
1976	JUN23	0821	34.100	97.400	OK	3	2.70	172.353	0.093703	0.003496
1976	JUN24	0802	34.100	97.400	OK	2	1.40	172.353	0.019758	0.000175
1976	JUN24	1528	35.600	103.300	NM	5		539.255	0.000000	0.000000
			34.160	97.400	OK	3	_	165.690	0.047557	0.000913
			34.930	96.220	OK		2.30	128.595	0.078251	0.001865
			35.560	95.680	OK		1.60	149.405	0.029043	0.000320
			34.750	96.120	OK		2.50	148.568	0.085809	0.002559
	OCT22		35.380	97.060			3.00	38.685	0.616041	0.031079
			35.850	97.320	OK		2.20	22.242	0.415699	0.008567
1976			35.230	96.380	OK		2.30	97.851	0.103400	0.002452
	DEC17			97.400	OK	F	2.90	172.353 166.259	0.000000	0.000000
	DEC19 FEB 4		34.920 34.065	95.730 97.370	OK OK	1 2	1.90	176.161	0.123508 0.035162	0.005744 0.000542
	FEB10		34.065	97.370			1.95	176.161	0.037331	0.000542
			36.263	97.437		2	1.62	68.793	0.065615	0.000000
	MAR 9			96.511			2.10	139.525	0.056670	0.001085
	MAR12			96.625			2.28	96.949	0.101912	0.001363
	MAR26	2137		97.370		3	2.35	176.161	0.060266	0.001528
	APR28			97.201		•	1.83	41.550	0.141109	0.001956
	MAY 22		36.240	97.246			1.42	65.994	0.053877	0.000479
1977			34.587	94.118			3.39	314.933	0.115748	0.009371
1977		.2335		93.898			2.63	332.981	0.044018	0.001540
	JUN 2		34.587	94.358			1.05	294.825	0.007515	0.000046
1977			34.612	94.087	AR		1.50	316.482	0.011982	0.000120
1977	JUN 3	0014	34.921	94.135	AR		1.19	300.910	0.008703	0.000062
1977	JUN 3	0135	34.587	94.118	ΛR		1.04	314.933	0.006942	0.000042
1977	JUN 3	0147			AΕ		0.66	314.933	0.004405	0.000017
1977	JUN 3		34.587		ΑR		0.78	314.933	0.005085	0.000023
1977	JUN 3	0758	34.587		ΑR		0.66	314.933	0.004405	0.000017
1977	JUN 3	0816	34.650	93.931			2.08	328.203	0.023122	0.000440
1977	JUN 7	2301		100.774			3.45	443.066	0.087801	0.007648
1977			32.858	100.774	TX		2.26	443.066	0.021120	0.000494
				97.358			1.97	178.809	0.037658	0.000627
1977			33.909	97.444			1.80	193.738	0.028310	0.000392
				100.401			2.48	463.497	0.026250	0.000783
			34.193	96.958			2.46	165.410	0.073310 0.023611	0.002096 0.000420
			35.337 35.476	94.040 96.304			2.02 1.64	299.675 94.737	0.023611	0.000420
			34.677	97.546			1.86	109.885	0.054243	0.000334
	AUG18		41.139	98.581			2.70	619.586	0.025407	0.000973
			33.947	95.243			2.49	268.467	0.046369	0.001384
			33.987	97.346			1.65	184.797	0.024824	0.000291
1977			36.394	97.072			2.11	85.863	0.094106	0.001804
			· · ·						<del> •</del>	<del></del>

Table 1. (continued)

YEAR	DATE	UTC	LAT DN	LON DW	ST	MM	MAG	DELTAkm	Ah %g	Vh cm/sec
1077	OCM 6	0036	35 030	07 767	^"		2 0 5	42 700		
	OCT 6 NOV 3	0036		97.767			2.05	43.709	0.174386	0.003086
				94.130			2.29	386.317	0.025178	0.000607
	NOV 25		37.958	95.864		4	2.19	287.725	0.030168	0.000647
	NOV 26			92.884		4	2.84	426.718	0.043950	0.001949
	NOV27		32.862 33.022	100.676			2.34	436.364	0.023608	0.000603
			40.408	100.842			2.79	434.878	0.040603	0.001705
	DEC 1			100.303			2.36	589.274	0.017798	0.000467
			40.732 35.449	99.846 97.927			2.71	605.951	0.026303	0.001018
			37.160				2.03	58.412	0.126667	0.002205
	DEC10			97.017			1.81	170.109	0.032716	0.000456
			37.095 36.971	97.007			1.80	163.147	0.033734	0.000465
			35.824	97.463			1.53	147.271	0.027103	0.000277
	JAN11			97.642			1.96	34.143	0.201432	0.003211
	JAN12		38.876 40.356	96.235				371.319	0.000000	0.000000
	JAN12		39.890	95.450	MO			548.223	0.000000	0.000000
			40.078	95.995	KS		2 72	485.518	0.000000	0.000000
	FEB10		34.712	100.321			2.72	557.624	0.028975	0.001132
			36.725	96.157	OK		1.54	149.041	0.027097	0.000280
			35.777	94.300 97.585	MO OK		2.04	296.835	0.024419	0.000444
	FEB21			99.003	OK		1.69 2.19	26.990 196.184	0.185298	0.002182
	MAR 3		35.086	96.278			2.13	114.080	0.044584 0.072134	0.000949
			34.699	95.033	OK		2.13	233.870	0.072134	0.001422 0.003900
			34.010	97.378	OK	2	2.55	182.288	0.033142	0.003900
			34.635	96.057	OK	2	2.31	161.556	0.062749	0.002340
	APR11		35.558	93.759	AR		1.90	322.789	0.002749	0.000296
	APR11			92.869	AR		1.97	403.254	0.016429	0.000238
	APR11			95.681	OK		1.74	183.693	0.027818	0.000360
	APR13		35.539	92.625	AR		1.75	425.309	0.011957	0.000159
	APR13	0343	34.351	96.820	OK		1.95	151.625	0.043502	0.000707
	APR14	2327	39.838	96.385	KS		1.73	472.716	0.000000	0.000000
	APR19		36.088	96.136	OK		1.47	118.018	0.031616	0.000301
		0813	34.586	96.293	OK		1.68	151.203	0.031575	0.000381
			34.572	93.977			1.87	327.481	0.018022	0.000331
	MAY 1		34.400	94.673			2.20	278.833	0.031524	0.000683
	MAY 4		35.588	96.345	OK		1.33	89.241	0.031524	0.000088
	MAY 7		42.310		NE	5	3.87	831.393	0.076400	0.010720
			35.525	97.910	ОК	1	2.26	54.221	0.179989	0.004035
	MAY18	0019	35.502	97.949	OK	3	2.74	58.311	0.296915	0.011330
	MAY18		35.601	97.828	OK	2	2.11	45.309	0.180631	0.003418
	MAY19		35.135	97.503	OK	4	2.02	59.333	0.123178	0.003418
	MAY19			97.367	OK		1.76	39.256	0.137505	0.002122
			40.110	100.320	NE		2.80	560.697	0.031710	0.001762
			39.138	96.295			1.93	398.208		
	MAY 28			96.293			0.94	117.850	0.015863 0.016786	0.000257 0.000089
,		J J L J	77.213	70 *T44	OI		U . 24	TT1.000	0.010/00	0.000003

Table 1. (continued)

YEAR	DATE	UTC	LAT DN	LON DW	ST	MM	MAG	DELTAkm	Ah %g	Vh cm/sec
1978	JUN16	1146	32,961	100.794	ТX	F	4.66	436.323	0.379746	0.125948
	JUN16				ΤX		3.44	456.015	0.084244	0.007261
1978	JUN22	0510	35.923	99.089	OK		2.00	161.432	0.043326	0.000745
1978	AUG 3	0035	36.689	100.162	OK		2.11	279.045	0.028282	0.000555
1978	AUG 6	0428	36.073	99.935	OK		2.16	239.255	0.035128	0.000726
1978		1207	34.127	97.463	OK		2.16	169.668	0.049878	0.001024
		1457	34.178	97.463	OK		1.40	164.015	0.020783	0.000184
1978		0516	36.155	95.275	OK		1.40	193.292	0.017578	0.000156
	SEP14			100.326	NE		2.90	591.944	0.033820	0.001613
	SEP26	2117	35.519	97.866	OK		2.15	50.578	0.169380	0.003358
	SEP27		35.519	97.843	OK		2.10	48.591	0.166194	0.003115
	SEP27	2056	33.883	97.477	OK		2.43	196.805	0.059235	0.001644
	OCT31	1205	35.458	94.297	AR		1.83	275.021	0.020528	0.000296 0.000000
	NOV 1		39.883	97.352	KS		2 62	470.371 259.237	0.056823	0.001978
1978		2306 2306		99.179 100.440	KS KS		2.63	419.237	0.000000	0.000000
1978		1118	38.492 34.676	96.063	OK		1.76	157.990	0.033227	0.000438
		1341		93.525	MO		2.42	530.701	0.033227	0.000596
	DEC10			95.125	OK		1.70	209.398	0.023201	0.000288
		2200		97.512	OK		1.96	184.539	0.036032	0.000594
		0530	34.080	97.462			1.92	174.871	0.036285	0.000572
			33.991	97.456	OK		2.08	184.704	0.041562	0.000783
1979			35.557	93.468			2.01	349.073	0.019967	0.000352
1979				93.215	AR		2.12	382.172	0.020768	0.000415
	JAN 8	1135		98.146	OK		2.12	126.577	0.064105	0.001252
1979	JAN24	0342	39.634	96.094	KS			455.861	0.000000	0.000000
1979	JAN 24	0515	33.985	97.434	OK		1.43	185.256	0.019027	0.000175
1979			34.022	97.381			2.07	180.962	0.041933	0.000781
1979		1024	35.483	94.568	OK		1.40	250.342	0.013502	0.000121
1979			34.916	97.333	OK		2.61	81.703	0.180142	0.005995
1979			34.830	96.062	OK		1.72	146.783	0.034142	0.000430
1979			34.672	97.157			2.49	109.805	0.115415	0.003384
1979		1423		96.092	OK		1.81	123.823	0.045231	0.000627 0.000000
1979		1956	39.257 39.134	95.891 92.671	MO		1.90	420.427 564.809	0.000000 0.010714	0.000169
1979							2.00	187.091	0.010714	0.000643
			33.969 37.137	97.446 97.135			1.60	166.152	0.026060	0.000288
			37.121	97.148			1.87	164.265	0.036429	0.000543
			35.421	97.851		2	1.68	53.544	0.091036	0.001075
			35.421	97.826			1.86	47.905	0.126506	0.001818
			35.781	97.650		•	1.42	32.333	0.111549	0.000978
			35.519	97.781		5	2.17	43.278	0.203380	0.004109
			35.689	97.923			1.62	53.707	0.084464	0.000933
			36.517	98.123			1.88	119.803	0.050870	0.000761
			35.377	98.100	OK		1.62	75.965	0.059302	0.000660

Table 1. (continued)

VES D	DAMG	TIMO	TAM DAT	TON DOT	C m	65 55	MAC	DELTAkm	7 h 9 g	Vh cm/soc
YEAR	DATE	UTC	LAT DN	LON DW	ST	PHP	MAG	DEDIAKII	Ah %g	Vh cm/sec
1979	MAR18	1733	35.410	98.115	ок		0.84	75.832	0.023348	0.000110
	MAR18		35.410		OK		1.01	75.832	0.028619	0.000162
		1739	35.410	98.115	OK		1.52	75.832	0.052705	0.000525
			35.410		OK		1.61	75.832	0.058702	0.000646
			35.344	98.053	OK		1.79	73.718	0.074950	0.001006
			35.384	98.110	OK		1.57	76.489	0.055466	0.000584
1979			35.439	98.118	OK		1.98	75.005	0.092450	0.001531
1979	MAR18	1314	35.410	98.116	OK		1.72	75.916	0.066889	0.000831
			35.418	98.108	ΟK		2.26	74.926	0.129412	0.002920
			35.443	98.126	ОК		2.04	75.554	0.098600	0.001745
			35.416	98.130	OK		2.02	76.872	0.094583	0.001638
		1913	35.418	98.155	OK		2.38	78.930	0.141681	0.003654
		1930	35.413	98.101	OK		2.16	74.332	0.115745	0.002338
	MAR18		35.406	98.110	OK		2.01	75.568	0.095102	0.001628 0.004830
	MAR18	2005	35.416	98.110	OK		2.48	75.173 75.019	0.167848 0.142241	0.004630
	MAR18 MAR18	2024 2044	35.420 35.379	98.110 98.124	OK OK	2	2.34 2.85	77.873	0.252164	0.010930
	MAR18	2107	35.429	98.114	OK	J	1.82	75.022	0.076315	0.001059
	MAR18		35.379	98.118	OK		1.76	77.373	0.068324	0.000894
	MAR18		35.394	98.108	OK		2.53	75.894	0.176476	0.005368
	MAR18	2208	35.396	98.126	OK		1.90	77.324	0.081437	0.001235
	MAR18		35.416	98.126	OK		1.85	76.532	0.077514	0.001112
	MAR18	2319	34.100	97.448	OK	3	2.34	172.570	0.060813	0.001524
	MAR18	2340	35.433	98.102	OK		2.04	73.849	0.100922	0.001785
1979	MAR19	0054	35.408	98.102	OK		2.01	74.813	0.096082	0.001644
1979	MAR19	0342	35.400	98.110	OK		2.46	75.813	0.162466	0.004574
1979	MAR21			96.349	OK		1.19	111.603	0.023937	0.000167
1979	MAR23		34.034	97.430	ΟK		1.29	179.800	0.016589	0.000130
1979	MAR23		34.022	97.440	OK		1.84	181.180	0.031800	0.000459
1979			35.361	98.108	OK		1.76	77.357	0.068838	0.000894
1979	MAR23		35.387	98.108	OK		1.93	76.192	0.085694	0.001343
1979		1043	35.605	97.974	OK		1.53	58.381 79.872	0.069647 0.105016	0.000698
1979 19 <b>7</b> 9	MAR23 APR 1		35.411 35.420	98.163 98.132	OK		2.14 1.73	76.892	0.103018	0.002078
			40.969	98.564			2.40	600.720		0.000503
			35.789	96.711			1.58	57.940	0.074517	0.000303
			35.923	97.480			1.92	33.212	0.197503	0.003011
			35.301	97.601			1.86	45.884	0.132192	0.001898
			34.027	97.470		3	1.89	180.798	0.033835	0.000516
			34.055	97.405		_	2.17	177.367	0.048245	0.001003
			36.207	97.330			1.44	61.893	0.058914	0.000535
			39.444	97.788			2.20	423.515	0.020582	0.000450
			40.144	100.348			2.50	565.107	0.021965	0.000673
			35.187	99.812	OK	3	2.94	230.572	0.092819	0.004541
1979	JUN12	1113	40.406	96.054	NE		1.80	540.095	0.009949	0.000140

Table 1. (continued)

YEAR	DATE	UTC	LAT DN	LON DW	ST	MM	MAG	DELTAkm	Ah %g	Vh cm/sec
1979	JUN15	0508	39.840	97.220	KS		1.90	465.689	0.013045	0.000205
			34.715	95.965			1.44	161.749	0.022115	0.000205
	JUN19		34.746	95.932	OK		1.76	161.879	0.032413	0.000427
1979	JUN25	0730	38.016	97.005	KS		1.60	264.511	0.016218	0.000181
1979	JUN 26	1304	39.296	96.016	KS		2.00	421.400	0.016282	0.000285
1979	JUN30	2046	39.937	97.274		4	3.10	476.359	0.053630	0.003177
1979	JUN30	2110	39.908	97.292	KS		1.40	473.179	0.007053	0.000064
	JUL 1		34.028	97.383			1.83	180.300	0.031578	0.000451
	JUL 1		39.952	97.286			2.00	478.027	0.014317	0.000252
1979	JUL 4		35.705	97.978	ОК		2.34	58.809	0.182333	0.004473
1979	JUL 7		34.879	95.814	OK		1.61	162.044	0.027057	0.000302
	JUL13		34.033	95.087			1.34	272.267	0.011535	0.000097
	JUL14	1832	39.526		KS	_	2.10	462.856	0.016678	0.000327
				100.287	NE		2.70	565.000	0.027913	0.001066
1979			-	100.345	NE	3	2.50	569.829	0.021779	0.000667
1979				100.333	NE		1.30	569.108	0.005183	0.000042 0.000067
1979				100.346	NE		1.50	569.431 569.966	0.006582 0.004073	0.000087
	JUL16		40.200	100.332 97.506	NE OK		1.10 2.50	49.288	0.264425	0.000027
	JUL24 JUL24			100.433			2.20	574.864	0.204423	0.000331
	JUL24		40.200	99.623			1.90	571.488	0.010586	0.000167
1979			33.967	97.549		5	2.74	188.078	0.089924	0.003513
	JUL31			97.305	OK	,	2.52	48.500	0.275321	0.008208
1979		0416					2.50	568.281	0.021840	0.000669
1979	AUG 2	1046	38.930	96.563			2.20	370.696	0.023578	0.000514
1979		0529		100.737	TX		2.57	441.203	0.030744	0.001012
1979		1029	35.683	98.005	OK		1.93	61.046	0.107430	0.001676
1979		0004	33.930	97.432	OK		2.35	191.351	0.055390	0.001407
1979	AUG13		40.113	100.502	NE		1.70	568.654	0.008374	0.000106
1979	AUG14	2359	40.173	100.343	NE		1.50	567.796	0.006601	0.000067
1979	AUG15	0645	40.145	100.339	NE		1.50	564.855	0.006636	0.00006 <b>7</b>
1979	AUG15	1607		100.441	NE		1.30	568.779	0.005186	0.000042
1979	AUG16		34.953	97.602	OK		1.85	81.283	0.072395	0.001047
	AUG19		35.203	97.445	OK		2.22	50.750	0.183550	0.003932
				100.337		4	2.20	564.169	0.015362	0.000338
			34.799	97.557			2.28	96.781	0.102092	0.002367
			35.429	97.871			1.87	54.735	0.111755	0.001628
1979			35.427	97.717			1.83	42.878	0.136653	0.001896
			39.391	95.892			1.50	434.586	0.008671	0.000087
	SEP13		35.217	99.362			3.37	190.162	0.189057	0.014321
1979			35.380	99.360			1.88	186.042	0.032471 0.102745	0.000490 0.001339
1979			35.493 35.369	97.882 97.952			1.77 1.90	52.854 64.346	0.102745	0.001339
			35.355	97.997			1.70	68.667	0.030222	0.001404
			35.435	97.997			1.69	63.524	0.077393	0.000927
1213	PILTO	0027	22.423	71.50I	OI		T • 02	004023	0.011333	0.000727

Table 1. (continued)

YEAR	DATE	UTC	LAT DN	LON DW	ST	MM	MAG	DELTAkm	Λh %g	Vh cm/sec
				,						
1979	SEP16	1042	35.455	97.905	OK		2.03	56.318	0.131474	0.002287
1979	SEP16	1107	35.355	97.989	OK		1.83	68.032	0.085336	0.001195
1979	SEP16	1557	35.343	97.997	ОК	4	2.48	69.317	0.182322	0.005238
1979	SEP16	2216	35.355	97.966	OK		1.87	66.216	0.092027	0.001346
1979	SEP17	1438	35.063	94.937	ΟK		1.81	226.463	0.024434	0.000343
1979	SEP17	2041	35.320	97.968	OK	4	2.45	68.389	0.178326	0.004955
19 <b>7</b> 9	OCT 6	1108	34.887	95.873	OK		1.49	157.038	0.024198	0.000237
1979	OCT19	1617	37.077	98.605	KS		2.18	195.345	0.044247	0.000932
1979	OCT19	2112	37.113	98.599	KS		1.85	198.283	0.029354	0.000429
1979	OCT21	0729	34.502	96.432	OK.		2.15	151.465	0.055332	0.001121
1979	110V 7	0554	35.510	97.888	OK		2.12	52.773	0.156471	0.003003
19 <b>7</b> 9	NOV11	1026	35.695	98.050	OK		1.92	65.186	0.099280	0.001534
1979	NOV16	0550	35.285	95.987	OK		1.31	128.130	0.024004	0.000192
1979	NOV19	0458	40.248	100.046	ИE		1.50	563.603	0.006651	0.000067
1979	NOV27	0910	35.630	98.408	OK		3.25	97.375	0.324102	0.021956
1979	NOV 29	2202	40.163	100.361	NE		1.90	567.568	0.010661	0.000168
1979	DEC 7	1417	39.694	97.619	KS		2.10	450.103	0.017160	0.000336
1979	DEC 9	2312	33.988	97.353	OK	3	2.51	184.692	0.069554	0.002106
1979	DEC10	0825	34.965	96.307	OK		1.46	119.997	0.030715	0.000289
1979	DEC14	1320	35.187	97.664	OK		1.90	59.680	0.106060	0.001600
1979	DEC15	0730	37.199	98.513	KS		1.87	202.026	0.029497	0.000441
1979	DEC16	1237	35.158	98.741	OK		2.45	138.999	0.086502	0.002438
1979	DEC 20	1458	36.367	97.379	OK		2.12	79.794	0.102633	0.001986

Note: Delta is the distance from the Arcadia site and Ah and Vh are the expected maximum horizontal ground velocity and acceleration at the site. Both Ah and Vh are printed as zero when the magnitude is not known. F in the intensity column indicated that the earthquake was felt but the intensity was not known. Dates and times are in Coordinated Universal Time (subtract six hours to obtain Central Standard Time; subtract one day from the date if the resulting CST is between 1800 and 2359 inclusive).