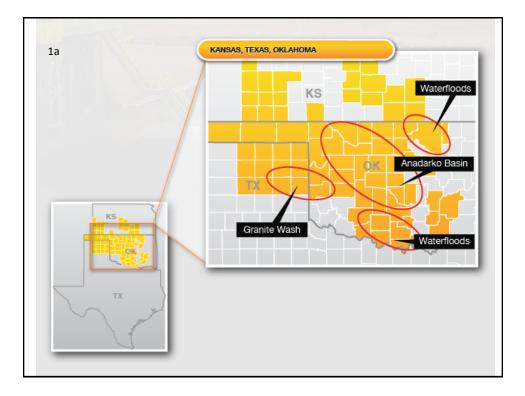
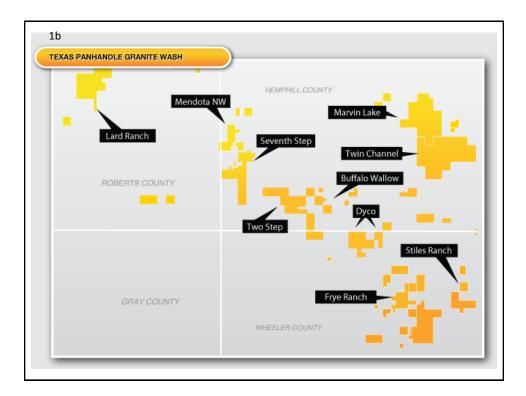
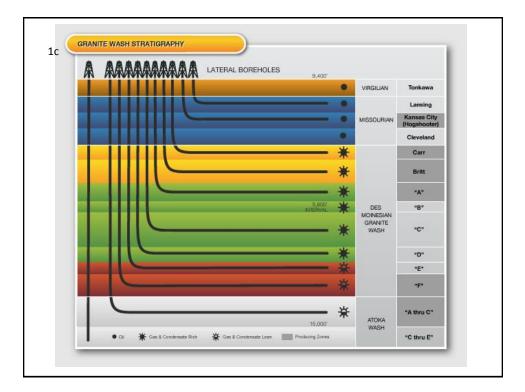
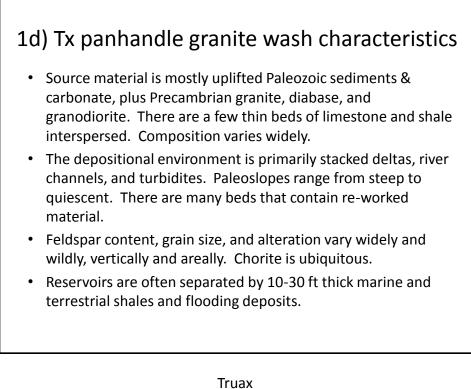


Twelve-Step Granite Wash Log Analysis
Groundwork
1. Geology discussions
2. Core & cuttings study
3. Log triage and repair
GR & neutron environmental corrections
5. Facies analysis
Calculations
6. VShale
7. Total & effective porosity
8. Saturation
9. Permeability & production
10. Flagging
11. Summations
12. Fraccability



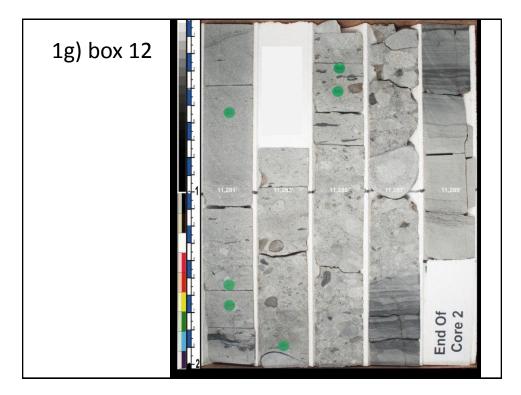


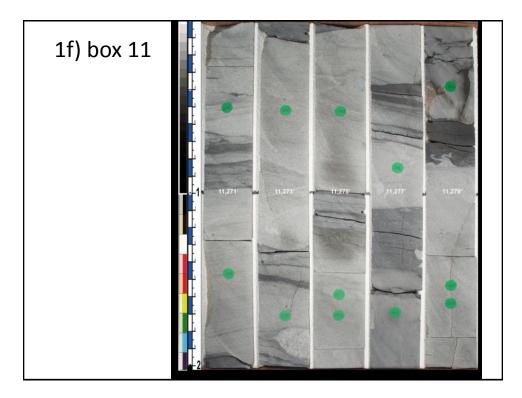


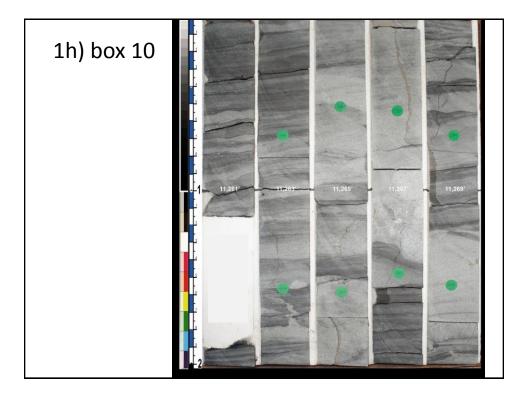


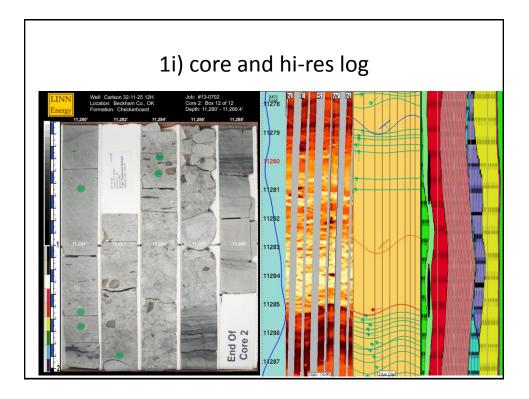
1e) Tx panhandle granite wash exploitation

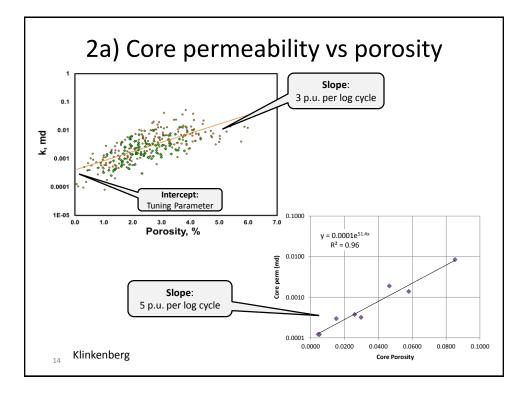
- There are about 100,000 vertical wells through the granite wash; many reach below to the Morrow and other horizons.
- Perms of present-day reservoirs are typically near 500 nd.
- Two or three 5000-ft laterals are typically drilled per section in one horizon. There are often stacked laterals.
- Slickwater fracs appear to be the most effective.
- Fraccing severely "bashes" adjacent producing wells where pressures have been lowered.
- Prospecting is done by sifting through production data and old logs.
- Recently there has been some drilling of "pilot" holes, or vertical holes before the turn, with coring and logging.

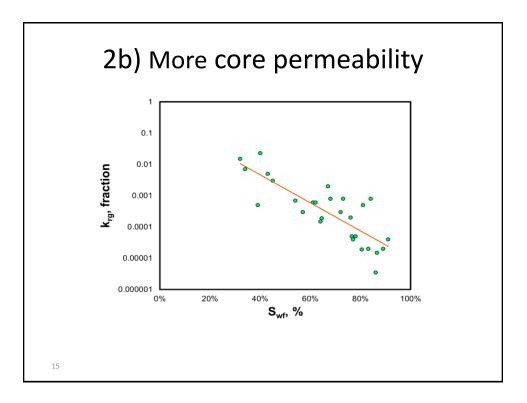


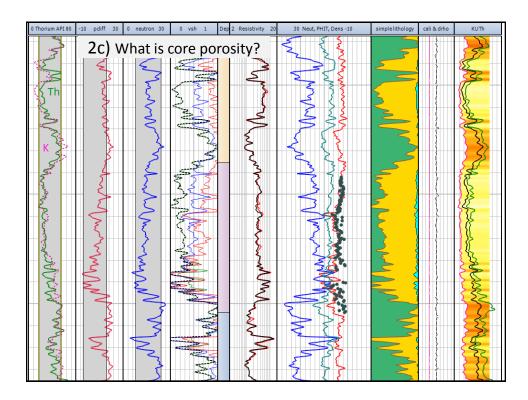


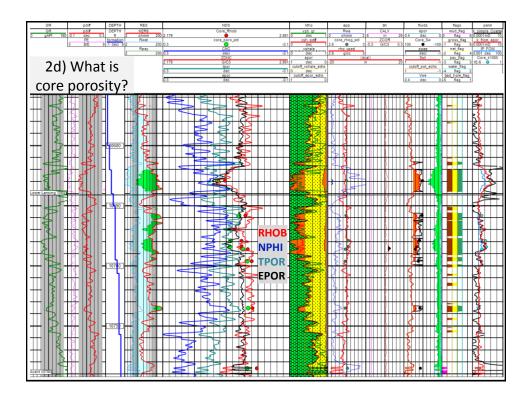


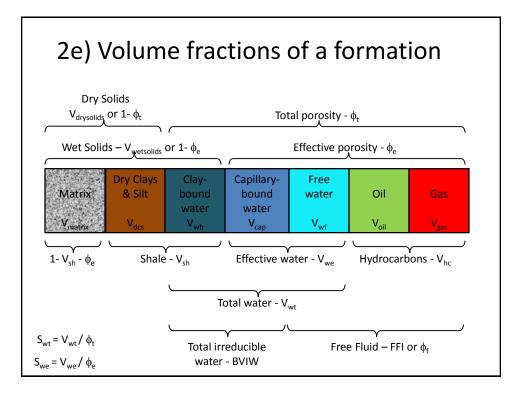


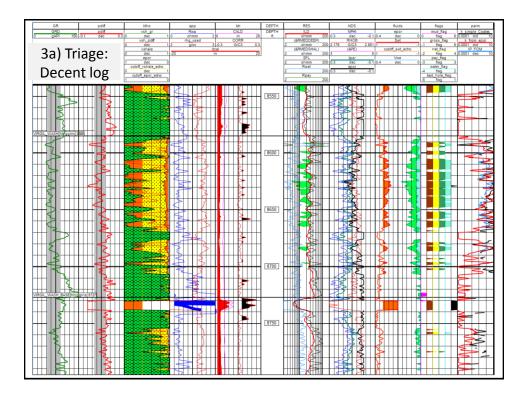


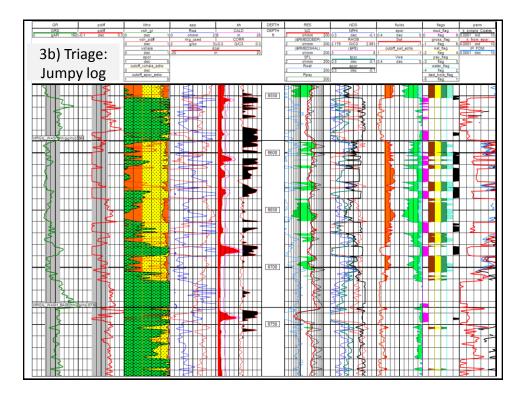


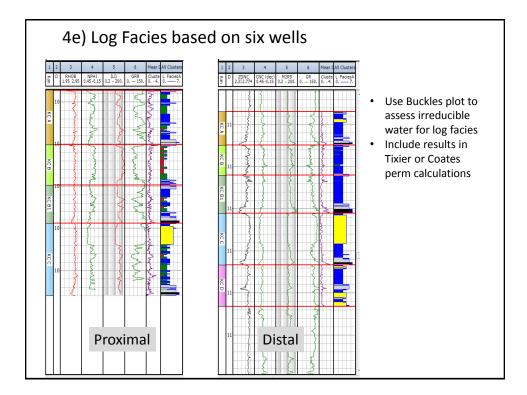




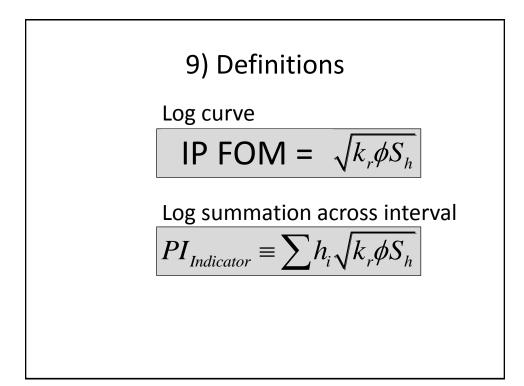


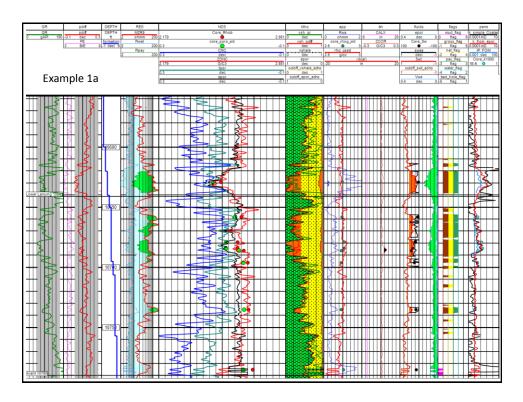


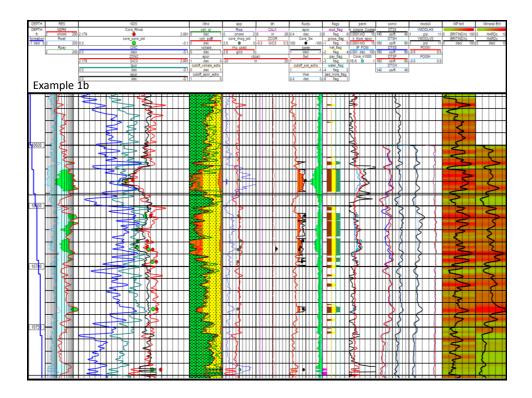


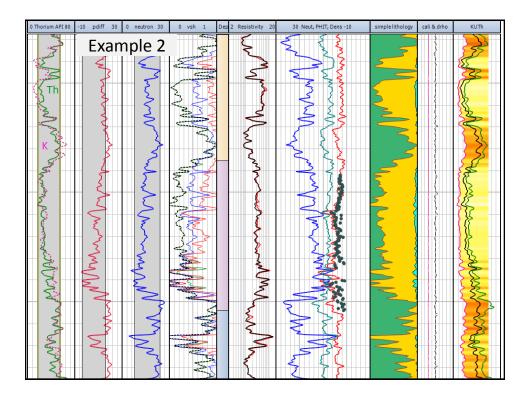


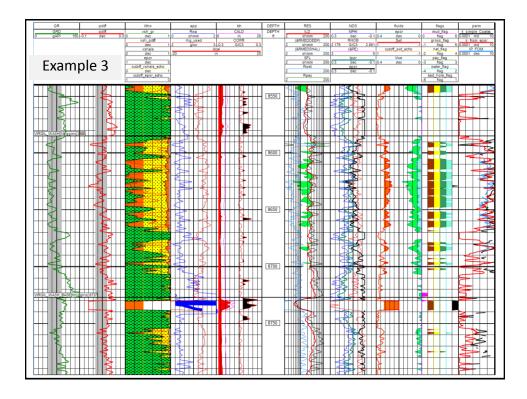
Twelve-Step Granite Wash Log Analysis Groundwork Geology discussions Core & cuttings study Log triage and repair GR & neutron environmental corrections Facies analysis Calculations VShale Total & effective porosity Saturation Permeability & production Flagging Summations Fraccability

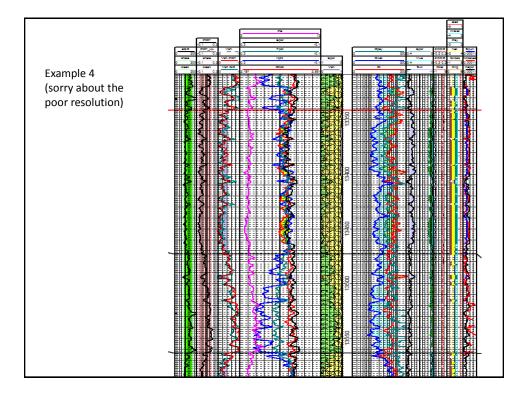












Reservoir Accounting

 $Q_{IP} \propto J_{lt} \Delta P$

 $J_{lt} \propto A_f \sqrt{k_r \phi c_{ti}} \frac{1}{\sqrt{\mu_i} B_i}$

 $q_i \propto x_{fi} h_i \sqrt{k_r \phi S_h}$

 $q_T \propto \sum h_i \sqrt{k_r \phi S_h}$

 $PI_{Indicator} \equiv \sum h_i \sqrt{k_r \phi S}$

 $k^* = \frac{1}{\phi^* S_1} \left(\frac{PI_{indicator}}{h} \right)$

SPE 139097, 162843, 166468

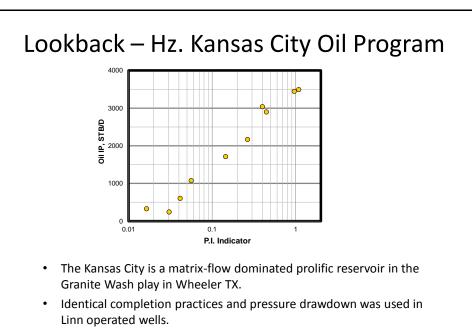
2

B

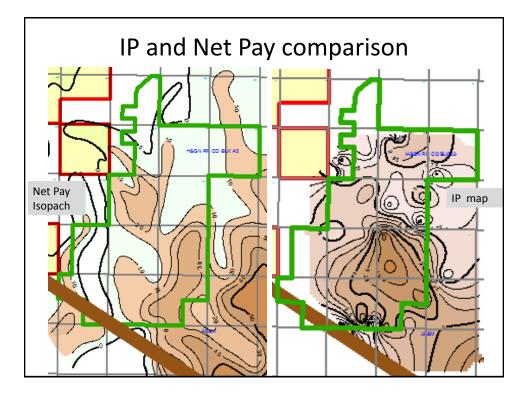
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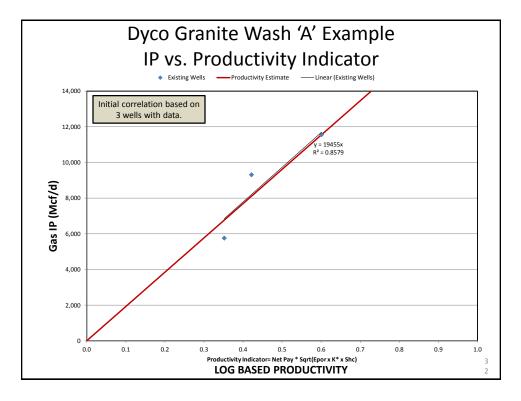
- 1. The initial production rates of a horizontal well in linear flow will be driven primarily by a lumped parameter J_{li} , which is dependent on both rock quality (perm k) and stimulation effectiveness (total frac surface area A_{i}), and pressure drawdown imposed on the well.
- For comparing wells of similar initial reservoir pressures we can skip normalizing the initial formation volume factor B_i, initial viscosity μ_i, and approximate initial total compressibility c_{ii} using hydrocarbon saturation S_i. The permeability k_i is effective to primary hydrocarbon phase.
- The flow rate of each flow unit (*i*) will be proportional to the net pay *h*, the fracture half-length propagated in each unit *x_{fr}* and its flow capacity. Fracture design related variations in *x_f* can be modeled as needed, for simplicity assume rectangular geometry – equal in all units.
- 4. Early life total flow rate in in tight reservoirs is the sum of the individual flow units; ignore crossflow. The total well rate is the sum of the net pay and flow capacity of each flow unit. For simplicity, the flow units can be the log sampling interval ½ feet intervals.
- 5. The productivity index indicator is defined and in LINE's experience is correlated to well performance; and can be used as a rock quality index.
- The upscaled* values of permeability can be calculated from the PI indicator for the tuning to well production results.

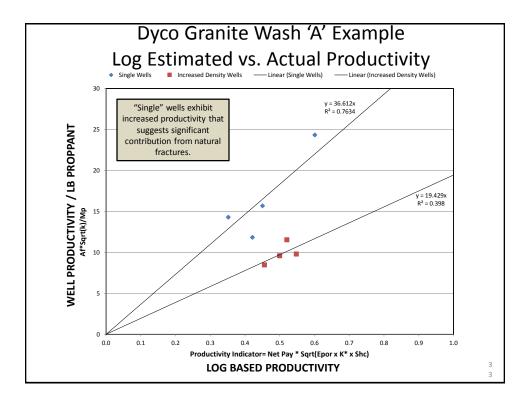
Review SPE 139097, 166468, and 166468 for theory and methods to normalize pressure drawdown, and completion practices.

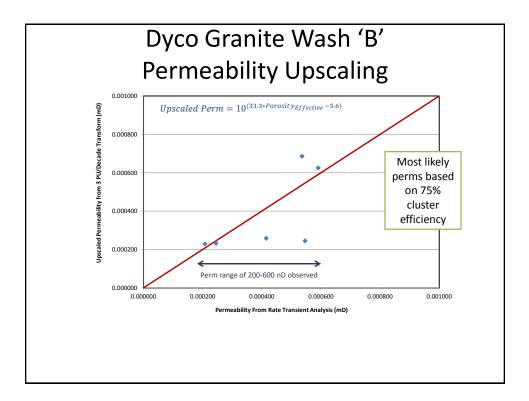


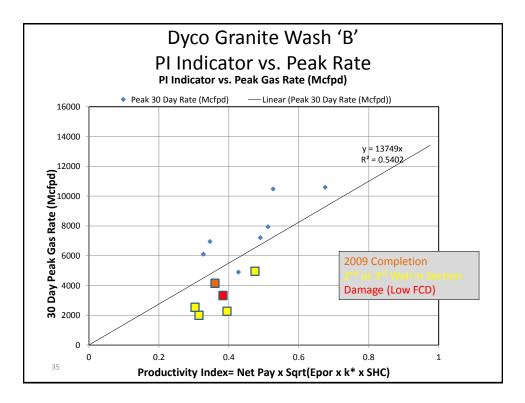
Clear correlation between highest oil production rates seen in these
 hz. wells compared to log-calculated productivity index.

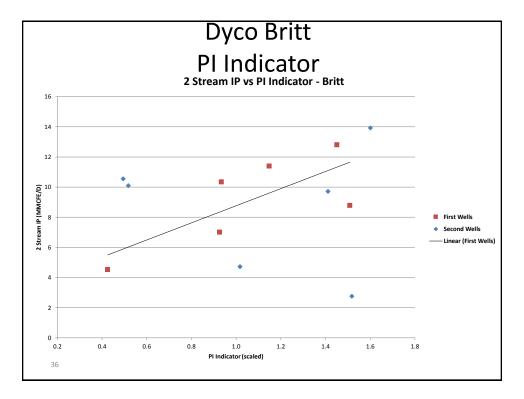












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